

# Advanced numerical studies of the neutralized drift compression of intense ion beam pulses

Adam B. Sefkow and Ronald C. Davidson

Plasma Physics Laboratory, Princeton University, Princeton, New Jersey 08543

Longitudinal bunch compression of intense ion beams for warm dense matter and heavy ion fusion applications occurs by imposing an axial velocity tilt onto an ion beam across the acceleration gap of a linear induction accelerator, and subsequently allowing the beam to drift through plasma in order to neutralize its space-charge and current as the pulse compresses. The detailed physics and implications of acceleration gap effects and focusing aberration on optimum longitudinal compression are quantitatively reviewed using particle-in-cell simulations, showing their dependence on many system parameters. Finite-size gap effects are shown to result in compression reduction, due to an increase in the effective longitudinal temperature imparted to the beam, and a decrease in intended fractional tilt. Sensitivity of the focal plane quality to initial beam temperature is explored, where slower particles are shown to experience increased levels of aberration compared to faster particles. A plateau effect in axial compression is shown to occur for larger initial pulse lengths, where aberrations due to longer drift lengths dominate increases in compression, indicating a trade-off between current compression and pulse duration. The dependence on intended fractional tilt is also discussed and agrees well with theory. A balance between longer initial pulse lengths and larger tilts is suggested, since both increase the current compression, but have opposite effects on the final pulse length, drift length, and aberration. Quantitative examples are outlined that explore the sensitive dependence of compression on the initial kinetic energy and thermal distribution of the beam particles. Simultaneous transverse and longitudinal current density compression can be achieved in the laboratory using a strong final-focus solenoid, and simulations addressing the effects of focusing aberration in both directions are presented.

## I. INTRODUCTION

Of the challenges encountered in developing heavy ion drivers [1] for warm dense matter and heavy ion fusion applications [2–4], one of the most significant is found in the final transport section leading to the target, where ion beam compression in space and time is required in order to achieve the necessary high intensities for striking the target [5, 6]. In other words, intense ion beam pulses must undergo simultaneous transverse and longitudinal bunch compression to a coincident focal plane in order to meet the requisite beam power on target [7]. Heavy ion drivers can deliver more intensity to the target per unit length of accelerator by greatly compressing intense ion charge bunches over short distances.

The Neutralized Transport Experiment [8] has demonstrated the feasibility of transverse compression of an intense ion beam by applying a radial focusing angle prior to neutralizing the beam’s space-charge and current in a plasma-filled drift region [9, 10]. When the plasma density  $n_p$  is much larger than the beam density  $n_b$  throughout the drift region, quasineutrality is maintained and the beam focuses ballistically to a small spot (few mm). When the neutralization level is very high, the focusing is emittance-dominated, meaning only the inherent temperature of the beam  $T_b$  limits the final beam radius  $r_b$ , due to chromatic aberration.

The Neutralized Drift Compression Experiment (NDCX) [11] currently studies longitudinal compression in a similar way, by providing plasma to neutralize the beam as it focuses in the axial direction. The primary component upgrade to the previous experiment is a lin-

ear induction accelerator [12] with one acceleration gap, which is also known as an induction module. The induction module employs a time-dependent waveform to modify the longitudinal velocity profile of the beam, in order to decrease the initial pulse length and increase the current of the beam. Such longitudinal focusing can also be emittance-dominated, provided that the accuracy of the imposed velocity tilt and the level of neutralization by the plasma are both high. The figures of merit are the compression ratio (maximum final to initial current) and the minimum pulse duration at focus. Compression ratios greater than 50 with full-width, half-maximum pulse lengths of  $< 5$  ns have been measured [13] in the NDCX device, and agree well with reduced numerical models and simulations [14]. Upcoming experiments will attempt to transversely focus a beam with an axial velocity tilt to a sub-mm spot size to a coincident focal plane. Particle-in-cell (PIC) simulations [7] and future experiments [15] seek to optimize the amount of current density compression, for a given set of experimental constraints.

The organization of this paper is as follows. The derivation of the equation for the induction module voltage waveform which imposes an ideal velocity tilt on a charge bunch is presented in Sec. II, along with other important parameters. The detailed physics and implications of acceleration gap effects and focusing aberration on optimum longitudinal compression are quantitatively reviewed using PIC simulations in Sec. III, and their dependence on many system parameters is examined. The roles of the finite-size acceleration gap and voltage waveform (Sec. III.A), beam temperature  $T_b$  (Sec. III.B), initial pulse length  $t_p$  and intended fractional tilt  $f$  (Sec.

III.C), and initial kinetic energy  $E_0$  and distribution (Sec. III.D) are evaluated. Implications pertaining to the simultaneous compression of intense charge bunches are also discussed (Sec. IV). Since imposing the velocity tilt results in the application of a time-dependent radial divergence to the ion beam (Sec. IV.A), a strong final-focus solenoid is situated near the end of the drift region in order to transversely focus the beam to a sub-mm spot size coincident with the longitudinal focal plane, and the compression (and aberration) dependence on beam radius  $r_b(t)$  entering the solenoid is explored (Sec. IV.B). A brief summary of the conclusions drawn from the paper is provided in Sec. V.

## II. IDEAL INDUCTION MODULE VOLTAGE WAVEFORM

There exists an ideal induction module voltage waveform that results in the imposition of a perfect velocity tilt on an ion beam with zero temperature across an infinitely thin acceleration gap for achieving maximal longitudinal compression at a desired focal plane [16]. In the classical limit of point particles, there is no upper bound on the longitudinal current compression (or lower bound on the pulse length) under the assumptions mentioned, since an ideal tilt will cause all of the beam particles to arrive at the focal plane at the exact same time. In reality, current density compression cannot be infinite due to beam temperature, laboratory constraints, and other physical realities that ultimately limit the achievable compression factors and pulse lengths.

In order for all the beam particles to coincidentally arrive at the same longitudinal focal plane, the central and tail portions of the charge bunch are required to travel a greater distance than the head portion in the same amount of time. The time-dependent velocity  $v_b(t)$  of the particles exiting the gap at time  $t$  should be [17]

$$v_b(t) = \frac{v_h}{1 - \frac{v_h t}{L_d}}, \quad (1)$$

where  $v_h$  is the decelerated velocity of the head of the beam,  $L_d$  is the drift length to the focal plane,  $t$  is evaluated from  $t = 0$  to  $t = t_p$ , and  $t_p$  is the initial pulse length of the beam, which is usually written as  $t_p = L_b/v_0$ , where  $L_b$  and  $v_0$  are the initial bunch length and velocity of the beam before entering the gap. The nonrelativistic energy of the beam is determined from  $E_b(t) = \frac{1}{2} m_b v_b^2(t)$ , where  $m_b$  is the mass of the beam particles, and the corresponding voltage waveform  $V(t)$  for the induction module that produces the desired  $E_b(t)$  is  $V(t) = \frac{1}{q_b} [E_b(t) - E_0(t)]$ , where  $q_b$  is the charge of the beam particles and  $E_0(t)$  is the initial energy of the beam ions (usually a constant) entering the gap. For maximum longitudinal compression, the tail of the charge bunch arrives at the focal plane at the same time as the head. The time and drift length required to reach maximal compression are

$$t_h^{foc} = \frac{v_t}{v_t - v_h} t_p \quad (2)$$

$$L_d = \frac{v_h v_t}{v_t - v_h} t_p, \quad (3)$$

respectively, where  $v_t$  is the accelerated velocity of the beam tail relative to  $v_0$  after it exits the gap at time  $t = t_p$ . Making the assumptions that the  $E_0$  entering the gap is constant in time, and that equal amounts of head and tail are decelerated and accelerated, respectively, allows the head and tail velocities to be defined as  $v_h \equiv v_0 (1 - f/2)$  and  $v_t \equiv v_0 (1 + f/2)$ , respectively, where the fractional velocity tilt  $f$  is defined as

$$f \equiv \frac{\Delta v_b}{v_0} = \frac{v_t - v_h}{v_0}. \quad (4)$$

Then, the time and drift length to longitudinal focus are

$$t_h^{foc} = \left( \frac{1}{f} + \frac{1}{2} \right) t_p \quad (5)$$

$$L_d = v_0 \frac{\left(1 - \frac{f}{2}\right) \left(1 + \frac{f}{2}\right)}{f} t_p = v_0 \left( \frac{1}{f} - \frac{f}{4} \right) t_p. \quad (6)$$

For the same value of  $E_0$ , larger tilts  $f$  give shorter  $L_d$  than smaller tilts, and longer initial pulse lengths  $t_p$  give longer  $L_d$  than shorter pulse lengths.

The time dependence of the velocity as the tilted beam exits the acceleration gap is

$$v_b(t) = v_0 \frac{\left(1 - \frac{f}{2}\right)}{\left[1 - \left(\frac{f}{1 + \frac{f}{2}}\right) \left(\frac{t}{t_p}\right)\right]}. \quad (7)$$

Then, the required ideal voltage waveform  $V(t)$  to time-dependently alter the charge bunch energy across the infinitely thin gap is given by [16]

$$V(t) = \frac{1}{2q_b} m_b v_0^2 \left( \left( \frac{\left(1 - \frac{f}{2}\right)}{\left[1 - \left(\frac{f}{1 + \frac{f}{2}}\right) \left(\frac{t}{t_p}\right)\right]} \right)^2 - 1 \right). \quad (8)$$

In experiments, the induction module is programmed to attempt the application of as near an ideal waveform as possible. The effects of an imposed non-ideal waveform on a beam pulse with finite temperature across an acceleration gap of finite length have been studied using reduced models [14]. In reality, the induced electric field encountered by the beam has significant extent in spatial and temporal dimensions, relative to the bunch and pulse lengths of the beam, rather than modifying the beam energy over an infinitely thin slice at one axial location, and gives rise to a number of complications.

### III. ACCELERATION GAP EFFECTS AND ABERRATION

Kinetic treatments are generally desired in order to realistically compute the experimentally achievable longitudinal compression ratios of ion beams with finite temperature  $T_b$ . Whether the resulting velocity tilt is nearly ideal or not, faster tail particles will overtake slower head particles, and a framework that properly retains the velocity distribution information is required to ascertain the current profiles in the vicinity of the longitudinal focal plane. Knowledge of the complete set of simulated current profiles  $I_b(z, t)$  of a charge bunch upstream and downstream of the focal plane is valuable when making comparisons to measurements, since diagnostics are situated at one particular axial location, and not necessarily at the focal plane.

In general, ion beam trajectories must be evaluated numerically by PIC techniques in order to take into account many of the effects that ultimately determine the quality of the focal plane. There is no universally valid analytical model for determining the expected current compression factor and pulse length, or even the current profile  $I_b(t)$ , at the focal plane because of the sensitive dependence on voltage waveform accuracy and finite-size gap geometry, most beam parameters, neutralization processes by the plasma, and other deleterious effects that decrease the compression. Simulations of intense beams with nonstationary density and velocity profiles propagating through plasma usually require PIC treatment due to the consideration of complex interactions, such as the nonlinear coupling between the transverse and longitudinal directions, instabilities, collisions between (or ionization of) beam, plasma, and neutral species, and 3D effects. Three-dimensional effects can include such topics as beam off-centering, misalignment of focusing and/or accelerating elements, and beam-beam effects in the interaction regions of colliders or heavy ion fusion drivers. All of the aforementioned issues, and any other nonlinear forces, can give rise to emittance growth of the beam and therefore affect the longitudinal compression dynamics.

Sets of PIC simulations are executed in order to quantitatively assess and classify the origin of different sources of longitudinal focal plane degradation involving the acceleration gap [18]. In order to isolate the effects of space-charge and plasma neutralization processes on the longitudinal dynamics from those arising strictly from the gap and initial beam parameters, the perveance and self-fields of the charge bunch are neglected by assuming perfect neutralization of the beam by the plasma in the simulations presented in this paper, which is a valid assumption in the limit  $n_p \gg n_b$  in the drift region (including the focal plane). All of the PIC results presented in this paper are from 2D  $\{r, z\}$  LSP simulations [19, 20], solve the electromagnetic field equations, treat all particle species as explicit and kinetic, resolve the plasma frequency  $\omega_p$  and cyclotron frequency  $\Omega_c$  of all species, are not susceptible to the so-called numerical Debye length instability

(because of an energy-conserving push), use a cloud-in-cell model, and conserve energy to good accuracy levels.

#### A. Dependence on gap size and voltage waveform

The derivation of the ideal velocity tilt assumed the beam encountered the imposed potential  $V(t)$  across an infinitely thin acceleration gap, had no thermal velocity distribution, and was entirely monoenergetic entering the gap. Realistically, an ion beam created in the laboratory must encounter a finite-size gap, always has some finite temperature, and might not be entirely monoenergetic entering the gap (or have the appropriate energy for the imparted voltage waveform). Practical engineering considerations such as voltage hold-off and the Volt-second capability of the induction module's magnetic flux must be taken into account, which limit the achievable induced electric field. Also, voltage waveform accuracy and its reproduction fidelity are experimental concerns. In order to make better comparison to measurements and provide insight into the physics of neutralized drift compression, a model needs to incorporate the actual spatial and temporal dependence of the electric field induced in the finite-size acceleration gap.

In order to ascertain the effects of the actual acceleration gap in the Neutralized Drift Compression Experiment (NDCX) on the longitudinal beam dynamics, two types of gap and voltage waveform for modifying the velocity distribution of an  $E_0 = 400$  keV  $K^+$  ion beam are studied (the maximum  $E_0$  achievable by the injector in experiments). The first gap is the "infinitely thin" approximation, which is recovered either by injecting the beam from a chosen plane with a prescribed velocity tilt as a time-dependent initial condition, or with an axial electric field strictly imposed over two adjacent grids. The second is the experimental finite-size gap, which begins at the conducting wall radius  $r_w = 3.8$  cm, is 3 cm long in the axial direction, and extends from  $z = -22$  cm to  $z = -19$  cm in the coordinate system here; the axial coordinate in the laboratory frame extends from  $z = -30$  cm to  $z = +150$  cm, where  $z = 0$  is the approximate starting location of the plasma. In experiments, the plasma drift length can be varied from 1 – 2.5 m. All simulations involving the 3 cm gap use an initial beam radius of  $r_b = 2$  cm and convergence angle  $\Delta\theta_r = -20$  mrad at the injection plane  $z = -30$  cm, the reason for which will be discussed shortly.

Two types of voltage waveform are employed for application of the velocity tilt over the two gaps. They are called the "sharp" and "smooth" waveforms and are illustrated in Fig. 1 [note that  $V(t) > 0$  results in an  $-E_z(z)$  in this model]. The  $V(t)$  shown corresponds to the ideal waveform for an  $E_0 = 400$  keV  $K^+$  beam with an intended fractional tilt  $f = 0.5$  over the initial pulse length  $t_p = 300$  ns, from  $t = 200$  ns to  $t = 500$  ns. The drift length to the longitudinal focal plane is predicted by Eq. (6) to be  $L_d = 78.7$  cm, or approximately  $z = +58.2$

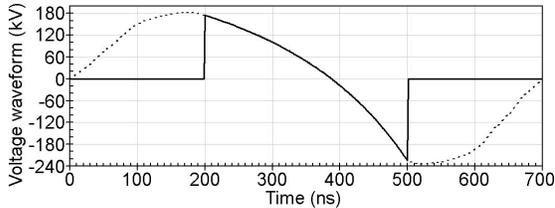


FIG. 1: Representative “sharp” (solid line) and “smooth” (dashed line) voltage waveforms used in particle-in-cell simulations. The  $V(t)$  shown [refer to Eq. (4.22)] corresponds to an ideal waveform for an  $E_0 = 400$  keV  $K^+$  beam with fractional tilt  $f = 0.5$  and initial pulse length  $t_p = 300$  ns, from  $t = 200$  ns to  $t = 500$  ns.

cm in this coordinate system. The “sharp” waveform ensures that only the ideal electric field is imposed for the duration of the beam’s initial pulse length. However, the experimentally realizable waveform requires ramp-up and ramp-down time for its voltage swing, and results in a waveform akin to the “smooth” one shown in Fig. 1. Therefore, the “smooth” waveform is the realistically achievable case. Simulations comparing both waveforms shed insight into the contribution to the longitudinal focusing dynamics from the suspectedly non-ideal extra voltage present in the “smooth” waveform (from  $t = 0 - 200$  ns and  $t = 500 - 700$  ns in Fig. 1).

A beam with an ideal velocity tilt results from applying the “sharp” waveform over an infinitely thin gap located at  $z = -20.5$  cm, which coincides with the center of the 3 cm gap. The initial cold  $K^+$  beam parameters are  $E_0 = 400$  keV,  $t_p = 300$  ns, and  $T_b = 0$  eV (corresponding to no emittance). Since the initial  $t_p$  is exactly equal to the intended pulse length to be compressed, the entire beam undergoes longitudinal compression. The perfectly velocity-tilted beam with zero temperature achieves maximal longitudinal compression at the focal plane  $z = +58.25$  cm. Since the code evolves point particles, no upper bound on the longitudinal current compression (or lower bound on the pulse length) exists in this case, except for the constraint of the finite time step. A compression ratio of 30,000 and minimum pulse length of 0.01 ns are achieved and are the expected classical limiting values, given the  $t_p = 300$  ns and discrete time step  $\Delta t = 0.01$  ns. Since the initial  $J_z$  is constant, the initial  $T_b$  is zero, the gap is infinitely thin, and an ideal velocity tilt is perfectly imparted, the axial beam number density profiles vary as  $v_z^{-1}(z, t)$  and the resulting current profiles in the laboratory frame at fixed axial locations are constant in time (square-shaped). Furthermore, the individual current profiles are symmetric about the center of the charge bunch in space and time, and generally about the focal plane. Lastly, the beam focuses at time  $t = 950$  ns, corresponding to  $t_t^{foc} = L_d/v_t = 450$  ns after the end of the “sharp” waveform. No difference in compression is observed using the “smooth” waveform instead because the extra voltage cannot act across an in-

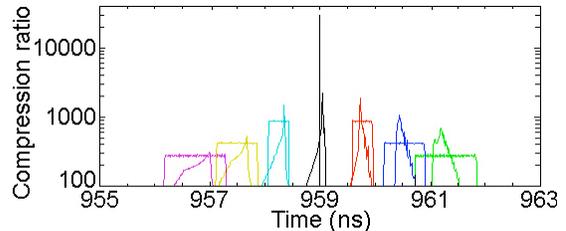


FIG. 2: (Color) Compression ratio  $I_b(t)/I_0$  (Log scale) in the laboratory frame at multiple axial locations near the focal plane ( $z = +59.5$  cm), in steps of  $\Delta z = 0.1$  cm. The beam is initialized with  $T_b = 0$  eV and encounters the “sharp” waveform across a 3 cm long gap. The results for the infinitely thin gap case (including the spatial and temporal offsets) are provided for comparison (constant current profiles).

finitely thin gap to cause the velocity of any excess beam to lie along the ideal tilt slope.

The simulation just described is repeated with the finite-size gap. In this case, the induced electric field varies as a function of space and time according to the boundary conditions and the “sharp” waveform, respectively. As revealed in Fig. 2, the cold beam suffers compression degradation compared to the ideal gap case. The compression factor reduces to 2200, and the full-width, half-maximum pulse length increases to  $t_{fwhm} = 0.03$  ns, as a sole result of the finite-size gap. Also, the beam focuses at the axial location  $z = +59.5$  cm at  $t = 959$  ns, approximately 1.25 cm downstream of the ideal gap focal plane. The additional 9 ns corresponds to the extra transit time required by the beam particles traveling at the average (initial) velocity  $v_0$ . For comparison, the simulation results using an infinitely thin gap are also provided in Fig. 2, with the spatial and temporal offsets included for clarity. More discussion of these results will follow after the description of another simulation.

Next, the “sharp” waveform is exchanged with the more realistic “smooth” waveform. Figure 3 presents the difference in the  $\{z, v_z\}$  phase space of the beam in both cases involving the finite-size gap, where the initial pulse length is much longer than the amount intended for longitudinal compression ( $t_p = 300$  ns). The axially compressing portion of the beam at this particular time ( $t = 820$  ns) is located in the region of negative slope, from approximately  $z = +36$  cm to  $z = +44$  cm. Decompressing portions of the charge bunch precede and follow the compressing region. Differences in shape are due to the presence of the extra voltage from the finite rise time and fall time of the “smooth” waveform.

The transit time of the beam particles across the finite-size gap is an important consideration, since it causes the particles to sample a significant temporal range of the voltage waveform. Here, particles moving at velocity  $v_0$  require approximately 75 ns, which is about 25% of the intended  $t_p$  for longitudinal compression, to cross the on-axis  $\Delta z \sim 10$  cm affected by the electric field in

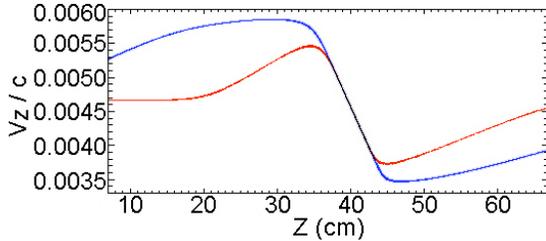


FIG. 3: (Color)  $\{z, v_z\}$  phase space at  $t = 820$  ns for the  $T_b = 0$  eV beam after application of the “sharp” waveform (red) and “smooth” waveform (blue) across the finite-size gap.

the gap region due to the boundary conditions. Since the waveform changes appreciably over the transit time, the integrated force experienced by each particle is less than the requisite amount for achieving the desired fractional tilt  $f$ . Particles within the gap near the beginning ( $t = 200$  ns, here) and end ( $t = 500$  ns, here) of the waveform do not encounter the appropriate integrated force required to participate in the intended velocity tilt, and contribute to the *decompressing* head and tail portions of the beam before and after the main compressing pulse, respectively. The spatial extents of the decompressing portions grow significantly later in time (as shown in Fig. 3) compared to the original separation, due to the relative expansion away from the main compressing pulse. It is apparent that the spatial and temporal “shapes” of the electric field in the gap (from the boundary conditions and waveform) impress themselves upon the phase space of the resulting beam.

The result in Fig. 3 demonstrates that the “sharp” waveform actually compresses less of the beam than the “smooth” waveform. The extra voltage in the “smooth” waveform acts on the excess beam to re-populate the low and high velocity space regions in the head and tail, respectively, of the intended tilt (the range of the intended  $f$  is  $v_z/c = \{0.0035, 0.0058\}$ ). Therefore, the extra voltage from the ramp-up and ramp-down of the “smooth” waveform is *advantageous* because of the extra integrated force. The “sharp” and “smooth” waveforms, applied across the finite-size gap, result in effective tilts of  $f \sim 0.3$  and  $f \sim 0.4$ , respectively, rather than the intended  $f = 0.5$  [however,  $L_d$  does *not* change according to Eqs. (3) or (6) due to the change in  $v_h$ ,  $v_t$ , and  $f$ ]. In other words, the finite-size gap effectively reduces the imparted  $f$  because of its inability to realize the maximum expected charge bunch head deceleration and tail acceleration, due to the temporal sampling of more waveform than intended by the particles.

The longitudinal compression results from the “sharp” and “smooth” waveform cases for the initial  $T_b = 0$  eV beam across the finite-size gap are shown in Fig. 4. In the linear plot, the difference in compression and pulse length is seen for the current profiles at equally-spaced locations near the focal plane. The maximum compression factor

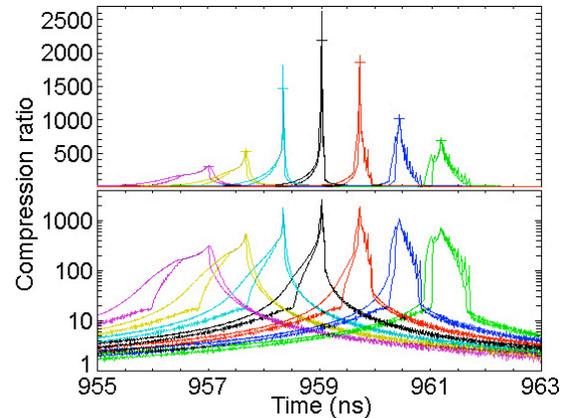


FIG. 4: (Color) Compression ratio  $I_b(t)/I_0$  comparison between “smooth” (top profiles) and “sharp” (bottom profiles) waveforms on linear (top) and Log (bottom) scales in the laboratory frame at multiple axial locations near the focal plane ( $z = +59.5$  cm), in steps of  $\Delta z = 0.1$  cm. The initial  $T_b = 0$  eV beams are tilted across the finite-size gap. Nonphysical horizontal bars are added on the linear scale plot to demarcate the excess compression in the “smooth” waveform case. The Log scale plot shows the increased amount of current in the pre-pulse of the “smooth” waveform case.

at the focal plane increases from 2200 to 2650 due to the larger effective tilt  $f$  achieved by the “smooth” waveform. However, more current contribution to the pre-pulse also occurs due to the extra voltage, as more clearly seen in the Log plot of Fig. 4, and the full-width, half-maximum pulse length at the focal plane increases by approximately 17% to 0.035 ns.

Figure 5 plots the  $\{z, v_z\}$  beam phase space, for an initially cold beam, at the focal plane for the case of the “sharp” waveform across an infinitely thin gap, and compares it to the “smooth” and “sharp” waveform cases across the finite-size gap. The cold beam with an ideal tilt from the infinitely thin gap results in an infinite compression (with a vanishing pulse length) in the point particle (and vanishing time step) limit, as discussed earlier and shown on the left of Fig. 5, where all of the beam particles arrive at the focal plane ( $z = +58.25$  cm) at the same time ( $t = 950$  ns). The center and right frames of Fig. 5 illustrate the effects of a finite-size gap and the use of “smooth” and “sharp” waveforms, respectively, on an initially cold beam.

Two important conclusions are drawn from the center and right plots of Fig. 5. First, the imposition of  $V(t)$  across a finite-size gap imparts velocity spread akin to an effective longitudinal temperature (emittance) on an otherwise initially cold beam with no space-charge. Therefore, a finite upper (lower) bound on the maximum compression (minimum pulse length) is set, due to chromatic aberration of the focal plane. The origin of this  $2D$  effect is found in the coupling of the transverse and longitudi-

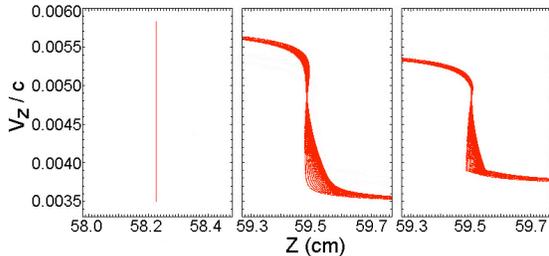


FIG. 5: (Color)  $\{z, v_z\}$  phase space at the focal plane for the  $T_b = 0$  eV beam using the “sharp” waveform across an infinitely thin gap (left), and “smooth” (center) and “sharp” (right) waveforms across the finite-size gap. Longitudinal focus occurs at  $z = +58.25$  cm and  $t = 950$  ns for the former case, and at  $z = +59.5$  cm and  $t = 959$  ns for the latter cases.

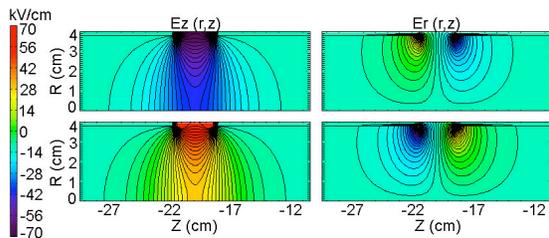


FIG. 6: (Color)  $\{r, z\}$  isocontour plots of  $E_z(r, z)$  at  $t = 200$  ns (top left) and  $t = 500$  ns (bottom left) and  $E_r(r, z)$  at  $t = 200$  ns (top right) and  $t = 500$  ns (bottom right) near the 3 cm acceleration gap. All plots are on the same linear scale.

nal dynamics of the beam as it traverses the finite-size gap. Radial components of the electric field exist wherever  $\partial E_z(r, z)/\partial z \neq 0$ , as illustrated in Fig. 6. The time-dependent nature of  $V(t)$  and the transit time across the gap imply an imbalance of integrated  $E_r(r, z, t)$  felt by each particle. In other words, the radial fields modify the  $v_r$  distribution of the beam non-uniformly. As a result, particles sample unequal amounts of integrated  $E_z(r, z, t)$  across the gap, instead of the same radially-independent integrated amount. During the compressing part of the voltage waveform [ $dV(t)/dt < 0$ ], beam particles at larger radii encounter a stronger imbalance of  $E_r$  fields, acquire more time-dependent changes to  $v_r$ , and are subsequently decelerated [for times when  $V(t) > 0$  and  $E_z(t) < 0$ ] or accelerated [for times when  $V(t) < 0$  and  $E_z(t) > 0$ ] in the axial direction *more* than particles initially closer to the  $r = 0$  axis. When the polarity switch from more axial deceleration to acceleration for particles farther off-axis occurs, it causes the X-shaped spread in the  $v_z$  distribution, as apparent in the center and right plots of Fig. 5. Therefore, due to the transverse movement of the particle trajectories within the gap, the beam acquires a velocity spread similar to temperature  $T_b$ .

The effective temperature increase acquired by the beam is dependent upon the gap geometry, voltage waveform, and beam parameters, such as axial velocity, ra-

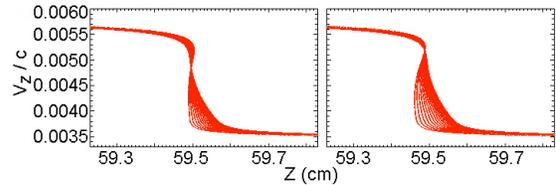


FIG. 7: (Color)  $\{z, v_z\}$  phase space at the focal plane for the  $T_b = 0$  eV,  $r_b = 2$  cm beam with a  $-20$  mrad convergence angle at  $z = -30$  cm (left) and no convergence angle (right) using the “smooth” waveform across the finite-size gap. The compression ratios and full-width, half-maximum pulse lengths at focus are 2650 and 0.035 ns compared to 1500 and 0.065 ns.

dius, convergence angle, and emittance, and will be quantitatively determined later. Note that the reduced velocity tilt  $f$  suffered by a beam crossing a finite-size gap should also be interpreted as an increase in effective longitudinal temperature, since the drift length  $L_d$  of the focal plane does not change with the reduced  $f$  value according to Eq. (6). As will be shown later, the presence of additional beam temperature decreases the compression ratio and increases the pulse length at focus without changing the axial location of the focal plane.

The effective increase in  $T_b$  is also dependent upon the transverse beam convergence entering the gap (quoted as  $\Delta\theta_r$  in radians as the beam radius  $r_b$  over the transverse focusing length  $L_r$ ), in addition to its radius. Intense beams generally have significant radially-converging angles, which are almost always much larger than the transverse velocity spread, as they exit the transport section and enter the gap, for transverse confinement as well as focusing. The  $E_r$  imbalance across the gap provides an average time-dependent radial defocusing force to all portions of the beam during the compressing [ $dV(t)/dt < 0$ ] part of the waveform [21]. Radial motion causes the sampling of unequal amounts of  $E_z(r, z, t)$  across the gap; therefore, a beam entering the gap with a trajectory that is radially converging will have some of its initial convergence offset by the time-dependent radial defocusing force. Then, the beam acquires less effective temperature (and compresses better) because it samples less integrated  $E_z(r, z, t)$  imbalance, compared to the case without an applied convergence.

The effect is shown in Fig. 7 for the beam parameters under previous consideration, with  $r_b = 2$  cm and a convergence angle of  $\Delta\theta_r = -20$  mrad. The beam’s  $v_r$  distribution varies radially as  $-v_r(r) = -v_z^0(r/r_b)(r_b/L_r)$  for  $r = 0$  to  $r = r_b$ . The case without a convergence angle suffered more gap-induced effective temperature increase due to increased radial movement within the gap compared to the case with an  $-20$  mrad angle at the plane of injection  $z = -30$  cm. The  $r_b = 2$  cm,  $\Delta\theta_r = -20$  mrad case is approximately the optimum radial initial condition for the average off-setting of the time-dependent defocusing force for the considered waveforms, and is used in all of the simulations involving the finite-size gap.

The second conclusion drawn from Fig. 5 is that the reduction of the intended tilt  $f$ , by the “smooth” and “sharp” waveforms acting across the finite-size gap, affects the faster tail particle velocities more than those in the slower head. From the left frame of Fig. 5, the expected minimum head and maximum tail velocities are  $v_z^h/c = 0.00350$  and  $v_z^t/c = 0.00583$ , respectively. From the center and right frames of Fig. 5, the realized maximum tail velocities are reduced compared to the infinitely thin gap case, more so than the difference between the minimum head velocities compared to the same. This effect occurs because accelerated tail particles have reduced transit times relative to the decelerated head particles, and therefore the integrated energy gain by the tail particles is not equal and opposite to the integrated energy loss by the head particles, since the energy modulation from the waveform is not imparted instantaneously.

In reality, not only does the acceleration gap have finite size, but a charge bunch has non-zero initial longitudinal temperature. Therefore, compression factors and pulse lengths at focus will be further reduced and increased, respectively, due to larger amounts of chromatic aberration relative to the cold beam cases. Also, beam emittance and aberration affect transverse compression as well by increasing the minimum achievable spot size. In order to quantify how finite beam temperature further reduces the established upper limits on longitudinal compression of a cold beam with NDCX-relevant parameters, additional simulations including the non-zero initial emittance of an ion beam are carried out.

## B. Dependence on beam temperature

The NDCX device is equipped with an injector capable of generating a high-brightness, low-emittance, and variable-perveance  $K^+$  ion beam with  $E_0 \leq 400$  keV of directed energy [8]. A beam’s brightness is proportional to the ratio of its current to the square of its transverse emittance, where the beam’s emittance is a measure of its area in phase space, and is related to its internal temperature according to [22]

$$\epsilon_n^{4rms} = 2 r_b \sqrt{\frac{T_\perp}{m_i c^2}}, \quad (9)$$

for a nonrelativistic, uniform round beam with a Maxwellian velocity distribution. Here,  $r_b$  is the beam radius,  $T_\perp$  is the transverse temperature, and  $m_i c^2$  is the rest energy of the beam. The normalized four-times-rms transverse effective emittance is given by Eq. (9) in units of m-rad (typically quoted in cm-mrad or mm-mrad). The longitudinal emittance is similarly defined with the longitudinal temperature  $T_\parallel$  and axial bunch length  $z_b$  instead. Liouville’s theorem ensures that the normalized emittance is conserved in the absence of nonlinear forces and coupling forces between different coordinate directions; in practice, Eq. (9) is a theoretical

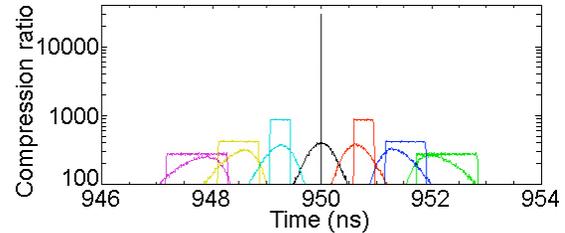


FIG. 8: (Color) Compression ratio  $I_b(t)/I_0$  (Log scale) comparison in the laboratory frame at multiple axial locations near the focal plane ( $z = +58.25$  cm), in steps of  $\Delta z = 0.1$  cm, for beams initialized with  $T_b = 0$  eV (constant current profiles) and  $T_b = 0.2$  eV (varying current profiles), both of which are ideally tilted using the “sharp” waveform across an infinitely thin gap.

lower limit because nonlinear dynamics, focusing aberrations, collisions, instabilities, and other effects can cause beam emittance growth in experiments [22]. Beams with low emittances are desirable because they experience less aberration during the focusing process.

In another simulation, the “sharp” waveform is employed over an infinitely thin gap and causes a fractional tilt of  $f = 0.5$  on a beam whose initial parameters are  $E_0 = 400$  keV and  $t_p = 300$  ns, with a  $T_b = 0.2$  eV Maxwellian distribution in both the transverse and longitudinal directions (corresponding to an emittance of  $9.3 \times 10^{-3}$  cm-mrad). The chosen beam temperature is consistent with measurements in the NDCX device. The current compression results near the focal plane are given in Fig. 8, alongside the cold beam results from Fig. 2 involving the same gap and waveform with no initial emittance. The maximum compression ratio for the  $T_b = 0.2$  eV case is 400 with a full-width, half-maximum pulse length of  $t_{fwhm} \sim 0.60$  ns.

The results in Fig. 8 show that the compression in the  $T_b = 0.2$  eV case is significantly affected by chromatic aberration, which causes a smearing of the longitudinal focal plane because of the axial velocity spread. Aberration increases the level of tolerance (at the cost of compression) for aligning a diagnostic or target with the focal plane: more  $T_b$  causes the peak current to vary less sensitively as a function of axial coordinate. The presence of temperature alone (even under this idealized case) results in asymmetric individual  $I_b(t)/I_0$  profiles in time about their respective peak values away from the focal plane. Slower head particles suffer increased levels of aberration (discussed below) and are sampled for longer durations at one particular axial location in the laboratory frame. They contribute more current to the pre-pulse for times before peak compression, whereas the opposite is true for the faster tail particles contributing to the post-pulse. After the focal plane has passed, the situation reverses and the pre-pulse is reduced relative to the post-pulse because the head particles are surpassed by the tail particles. Since the exact amount of initial

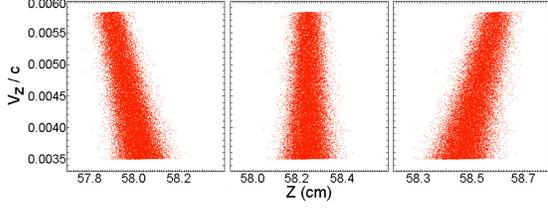


FIG. 9: (Color)  $\{z, v_z\}$  phase space for the  $T_b = 0.2$  eV beam, using the “sharp” waveform across an infinitely thin gap, 2 ns before arrival at the focal plane (left), at the focal plane (center), and 2 ns after passing the focal plane (right). Focus occurs at  $z = +58.25$  cm and  $t = 950$  ns.

beam pulse is perfectly tilted in this case, the profiles and the envelope of the peak current (from one profile to the next) are symmetric about the focal plane itself.

Returning to Figs. 2 and 4, the profiles in those plots are asymmetric due to the effective non-uniform longitudinal temperature imparted to an initially cold beam by the finite-size gap (refer also to Figs. 5 and 7). Likewise, the individual current profiles and the envelope of the peak current are not generally symmetric about the focal plane in those figures because more than the prescribed initial pulse length  $t_p = 300$  ns (according to the waveform) of beam is used. Downstream of the focal plane, the tail of the beam passes the head, causing the formation of different current profile features due to the multiple-valued nature of the  $\{z, v_z\}$  beam phase space at fixed  $z$  (similar to a Z-shape, if one considers the after-focus analogs of Figs. 3 and 5).

The  $\{z, v_z\}$  phase space 2 ns upstream of the focal plane, at the focal plane, and 2 ns downstream of the focal plane for the  $T_b = 0.2$  eV case using the “sharp” waveform across an infinitely thin gap are presented in Fig. 9. The distance traveled in 2 ns by the beam is approximately 0.2 cm; therefore, the yellow, black, and dark blue current profiles of the  $T_b = 0.2$  eV case in Fig. 8 are directly related to the left, center, and right frames of Fig. 9, respectively. Inspection of the two figures highlights the contribution of the velocity distribution (Maxwellian, here) from an ideally tilted beam to the shape of the current profile at a fixed location. Additional simulations regarding the role of the type of thermal distribution on the current compression will be discussed later.

A significant effect apparent in Fig. 9 is that slower head particles suffer more aberration due to finite- $T_b$  effects during the longitudinal focusing process, a result of the fact that the thermal velocity is always a greater fraction of head velocities compared to those in the tail. The contribution of chromatic aberration for an ion beam with finite emittance (which has been ideally velocity-tilted) to the temporal smearing of the focal plane can be calculated as follows.

Consider an ion beam with a Waterbag axial velocity distribution and thermal velocity  $v_{th} \ll v_0$ , where the so-called Waterbag distribution is one with uniform-

density and equally populated between  $v_0 - v_{th}$  and  $v_0 + v_{th}$ . The effective drift length to the focal plane can be calculated from Eq. (3) to be

$$L_d^{h+} = \frac{(v_h + v_{th}) v_t}{v_t - (v_h + v_{th})} t_p, \quad (10)$$

for the head particles moving with the slightly faster velocity  $v_h + v_{th}$  and

$$L_d^{h-} = \frac{(v_h - v_{th}) v_t}{v_t - (v_h - v_{th})} t_p, \quad (11)$$

for the head particles moving with the slightly slower velocity  $v_h - v_{th}$ . Then, the focal plane is no longer infinitely thin at one axial location  $L_d$  downstream of the gap, but is smeared about that location due to the beam’s temperature. The width of the range about  $L_d$  for the head of the charge bunch is

$$w^h \equiv L_d^{h+} - L_d^{h-} = 2 \frac{v_t^2}{(v_t - v_h)^2 - v_{th}^2} v_{th} t_p. \quad (12)$$

Similarly, the intended focal plane takes on a range of values whose width about  $L_d$  for the tail of the charge bunch is

$$w^t = 2 \frac{v_h^2}{(v_t - v_h)^2 - v_{th}^2} v_{th} t_p. \quad (13)$$

The excess aberration suffered by the slower head particles compared to the faster tail particles is then

$$w^h - w^t = 2 \frac{v_t^2 - v_h^2}{(v_t - v_h)^2 - v_{th}^2} v_{th} t_p, \quad (14)$$

and can be rewritten in terms of the initial beam velocity  $v_0$  and the fractional tilt  $f$ , using the definitions of  $v_h$  and  $v_t$  and their associated assumptions, as

$$w^h - w^t = \frac{4}{f} \frac{1}{1 - (v_{th}/v_0)^2} v_{th} t_p. \quad (15)$$

The effective longitudinal temperature of a Waterbag distribution is defined as

$$T_W \equiv m_b \int_{-v_{th}}^{+v_{th}} \frac{dv}{2 v_{th}} \mathbf{v}^2 = \frac{1}{3} m_b v_{th}^2, \quad (16)$$

whereas the temperature of a Maxwellian distribution is defined as

$$T_M \equiv m_b \int_{-\infty}^{+\infty} \frac{d\mathbf{v}}{\sqrt{2\pi} v_{th}} \mathbf{v}^2 \exp\left(-\frac{\mathbf{v}^2}{2 v_{th}^2}\right) = m_b v_{th}^2, \quad (17)$$

and  $T_M = 3 T_W$  for the same value of  $v_{th}$ . To analyze PIC simulations involving beams with Maxwellian distributions, the factor of  $\sqrt{3}$  in  $v_{th}$  ( $v_{th}^M = v_{th}^W/\sqrt{3}$ ) should be taken into account in Eqs. (10) to (15).

For the parameters of the simulations presented in Figs. 8 and 9, the widths  $w^h$  and  $w^t$  about  $L_d$  are

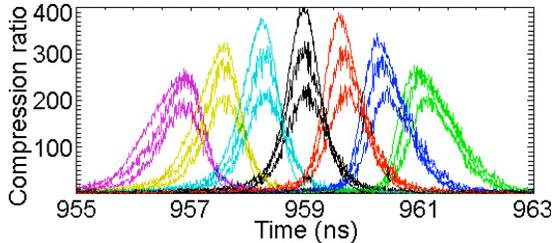


FIG. 10: (Color) Compression ratio  $I_b(t)/I_0$  comparison between “smooth” (middle profiles) and “sharp” (bottom profiles) waveforms in the laboratory frame at multiple axial locations near the focal plane ( $z = +59.5$  cm), in steps of  $\Delta z = 0.1$  cm. The beams initialized with  $T_b = 0.2$  eV are velocity-tilted across the 3 cm long gap. The infinitely thin gap case results (including the spatial and temporal offsets) from Fig. 8 are provided for comparison (top profiles).

0.151 cm and 0.054 cm, respectively, and agree well with the center frame of Fig. 9, which quantitatively shows the same 2.8 ratio of widths ( $w^h/w^t$ ) between the slowest and fastest particles. The full-width, half-maximum pulse length of the ideally-tilted beam with finite temperature at the focal plane (including aberration) is approximately equal to the weighted average

$$t_{fwhm} = \frac{1}{2} \left[ \frac{\left(\frac{w^h}{v_h}\right) w^h + \left(\frac{w^t}{v_t}\right) w^t}{w^h + w^t} \right], \quad (18)$$

which is  $t_{fwhm} = 0.58$  ns for the parameters here, in close agreement with the full-width, half-maximum pulse length of  $t_{fwhm} \sim 0.60$  ns plotted in the black current profile in Fig. 8 for the  $T_b = 0.2$  eV case.

Two additional simulations are executed in order to compare the compression results from the “sharp” and “smooth” waveforms imposed over the finite-size gap to the simulation involving the “sharp” waveform over an infinitely thin gap. The current profiles near the focal plane using the two waveforms applied to the  $T_b = 0.2$  eV beam over the finite-size gap are shown in Fig. 10 on a linear scale and are accompanied by the infinitely thin gap results of the same  $T_b = 0.2$  eV beam (previously plotted on a Log scale in Fig. 8). The aforementioned spatial and temporal offsets between the two gaps are included for clarity. As before, the “smooth” waveform effectively compresses more beam than the “sharp” waveform acting over the finite-size gap. The maximum compression ratio and full-width, half-maximum pulse length for the infinitely thin gap case are 400 and  $t_{fwhm} \sim 0.6$  ns, respectively. The corresponding “sharp” and “smooth” waveform results over the finite-size gap are approximately 235 compared to 320, and 0.65 ns compared to 0.70 ns, respectively. The differences in the finite-size gap cases relative to the infinitely thin gap case are due to the decreased effective tilts  $f$  (acting as effective temperature increases), compared to the intended  $f = 0.5$ , and associated increased levels of aberration.

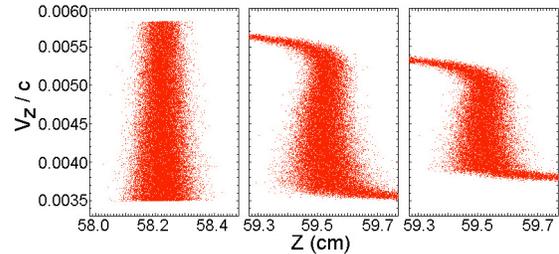


FIG. 11: (Color)  $\{z, v_z\}$  phase space at the focal plane for the  $T_b = 0.2$  eV beam using the “sharp” waveform across an infinitely thin gap (left), and “smooth” (center) and “sharp” (right) waveforms across the finite-size gap. Focus occurs at  $z = +58.25$  cm and  $t = 950$  ns for the former case, and at  $z = +59.5$  cm and  $t = 959$  ns for the latter cases.

The  $\{z, v_z\}$  beam phase space for the three cases described above at the longitudinal focal plane are provided in Fig. 11, and should be compared to the complimentary  $T_b = 0$  eV case results in Fig. 5. The two main effects of the finite-size gap are evident again in these simulations with an increased axial velocity spread. The slower head particles experience more aberration relative to the faster tail particles, and the decrease in maximum tail velocities from the ideal case is relatively larger than the corresponding increase in minimum head velocities from the ideal case. The tilt is again reduced from the intended  $f = 0.5$  to  $f \sim 0.4$  and  $f \sim 0.3$  for the “smooth” and “sharp” waveform cases, respectively, across the finite-size gap. Due to the initial  $T_b$  increase, the compression factors for the “sharp” and “smooth” waveforms across the finite-size gap precipitously drop from 2200 to 235 and 2650 to 320, respectively, and the full-width, half-maximum pulse lengths increase from 0.03 ns to 0.65 ns and 0.035 to 0.70 ns, respectively. The reduction in  $f$  causes the apparent increase in effective longitudinal  $T_b$ .

Numerical simulations involving a range of initialized Maxwellian longitudinal temperatures, for the case of the “smooth” voltage waveform across the finite-size gap, investigate the dependence of the current ratio on the initial emittance of the charge bunch. The initialized temperatures are  $T_b = 0.1$  eV, 0.2 eV, 0.4 eV, 0.8 eV, and 1.6 eV. The compression ratios achieved at the focal plane and the full-width, half-maximum pulse lengths are presented in Table I. The data in Table I correspond to the peak current profiles for those cases plotted together in Fig. 12 for comparison. The  $T_b = 0$  eV case is included in Table I and Fig. 12 for reference.

From Table I, the compression factor decreases and the minimum pulse length increases with an approximate square root dependence on the initial beam temperature ( $T_b^{-0.48}$  and  $T_b^{0.5}$ , respectively) as expected, since  $t_{fwhm} \sim v_{th} \sim \sqrt{T_z}$  according to Eq. (18) for  $v_{th} \ll v_h, v_t$ . The minimum full-width, half-maximum pulse length of a beam, which acquires an ideal velocity tilt across an infinitely thin gap and is perfectly neutral-

TABLE I: Compression dependence on initial  $T_b$  for  $E_0 = 400$  keV,  $t_p = 300$  ns, and  $f = 0.5$  using the “smooth” waveform across the 3 cm long gap.

$T_b$	$I_b^{max}/I_0$	$t_{fwhm}$	$t_{fwhm}$ [Eq. (18)]	$T_b^{inf}$ [Eq. (18)]
0 eV	2650	0.035 ns	0 ns	$7.5 \times 10^{-4}$ eV
0.1 eV	430	0.51 ns	0.41 ns	0.16 eV
0.2 eV	320	0.70 ns	0.58 ns	0.30 eV
0.4 eV	230	1.01 ns	0.81 ns	0.62 eV
0.8 eV	160	1.40 ns	1.15 ns	1.19 eV
1.6 eV	115	2.05 ns	1.63 ns	2.55 eV

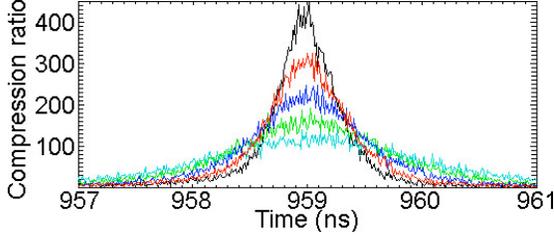


FIG. 12: (Color) Compression ratio  $I_b(t)/I_0$  comparison using the “smooth” waveform across the finite-size gap in the laboratory frame at the focal plane ( $z = +59.5$  cm) for initialized beam temperatures of  $T_b = 0.1$  eV (black),  $0.2$  eV (red),  $0.4$  eV (dark blue),  $0.8$  eV (green), and  $1.6$  eV (light blue).

ized, will be limited by the initial longitudinal temperature (emittance) according to Eq. (18). The predicted  $t_{fwhm}$  from that equation is shown in Table I. Although Eq. (18) includes the linearly-weighted average effect of the aberration experienced by all the beam particles, the equation does not include the finite-size gap or “smooth” waveform effects (both of which increase the beam’s effective temperature), as shown by the discrepancy between the third and fourth columns of Table I. Note that the difference between those columns also increases approximately with the square root of the initial  $T_b$ .

The inferred initial beam temperatures  $T_b^{inf}$  required to produce the value of  $t_{fwhm}$  from the PIC simulations using Eq. (18) are presented in the fifth column of Table I. The inferred temperatures are  $55\% \pm 5\%$  higher on average than the initial  $T_b$  used in simulations involving the 3 cm gap. The elevated values indicate the required presence of an additional constant ( $\sqrt{1.55}$ , here) in the  $v_{th}$  variable of Eqs. (12) and (13), in order to take into account the combined effects of the gap size and “smooth” waveform, for the set of parameters considered here. Recall that the infinitely thin gap case results in  $t_{fwhm} = 0.6$  ns, and the finite-size gap with a “smooth” waveform case results in  $t_{fwhm} = 0.7$  ns for  $T_b = 0.2$  eV, whereas Eq. (18) predicts  $t_{fwhm} = 0.58$  ns. Therefore, 17% of the temperature discrepancy is due to error in the equation (the averaging procedure linearly weights the velocities from  $v_h$  to  $v_t$ , but the tilt deviates from linearity later in the pulse in this case) and 83% of the temperature discrepancy is due to the increased

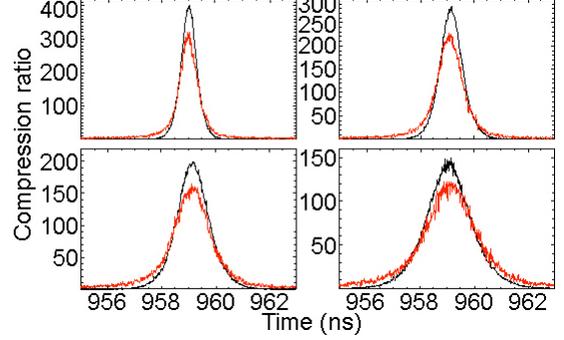


FIG. 13: (Color) Compression ratio  $I_b(t)/I_0$  comparison between the “sharp” waveform across the infinitely thin gap (black) and “smooth” waveform across the finite-size gap (red) in the laboratory frame at the focal plane (including the temporal and spatial offsets) for initialized  $T_b = 0.2$  eV (top left),  $T_b = 0.4$  eV (top right),  $T_b = 0.8$  eV (bottom left) and  $T_b = 1.6$  eV (bottom right).

effective temperature from the gap and waveform. Additional simulations involving other acceleration gap sizes only support a weak dependence on the length of the gap. However, the gap size and transit time of the particles should be considerably smaller than the initial bunch length  $L_b$  and pulse length  $t_p$ , respectively, for effectively imparting an intended fractional tilt  $f$ .

The amount of effective temperature imparted to an  $E_0 = 400$  keV beam with non-zero  $T_b$  as it encounters the “smooth” waveform for  $t_p = 300$  ns and  $f = 0.5$  across a finite-size gap can be determined by comparing to cases involving an infinitely thin gap. As shown in Fig. 13, four cases of initial  $T_b$  compare the case of the finite-size gap employing the “smooth” waveform to the infinitely thin gap case. Simulations initialized with  $T_b = 0.2$  eV,  $T_b = 0.4$  eV,  $T_b = 0.8$  eV, and  $T_b = 1.6$  eV each result in an approximate 20% relative decrease in maximum compression ratio and increase in full-width, half-maximum pulse length for the finite-gap and “smooth” waveform case compared to the infinitely thin gap case, as plotted in Fig. 13. Therefore, the effective longitudinal temperature difference between the two cases, due to the reduced  $f$  from finite-size gap and “smooth” waveform effects, is approximately 45% ( $\sqrt{20\%}$ ) and in very good agreement with the previous results, which state that the compression factor decreases with the square root of increasing  $T_b$ . As in the previous paragraph, the inferred  $T_b^{inf}$  are  $\sim 55\%$  higher on average in Table I, and  $\sim 83\%$  of that discrepancy ( $\sim 45\%$ ) is due to the effects of the finite-size gap and “smooth” waveform. As a check, simulations comparing  $T_b = 0.1$  eV in the finite-size gap case to  $T_b = 0.145$  eV in the infinitely thin gap case confirm the same compression result. In summary, for the parameters considered here, the 3 cm gap and “smooth” waveform together add the equivalent of approximately 45% of the initial  $T_b$  to the resulting effective longitudi-

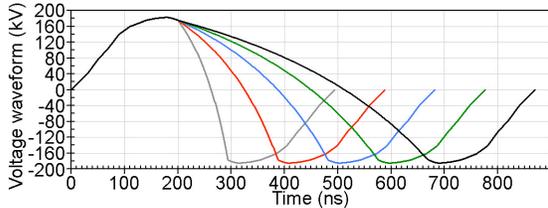


FIG. 14: (Color) “Smooth” waveforms  $V(t)$  for  $E_0 = 400$  keV,  $f = 0.5$ , and  $t_p = 100$  ns (gray),  $t_p = 200$  ns (red),  $t_p = 300$  ns (blue),  $t_p = 400$  ns (green), and  $t_p = 500$  ns (black).

nal emittance by reducing the achieved  $f$  relative to the intended  $f$ , and coupling the transverse and longitudinal phase space as the beam traverses the gap.

Analytical neutralized drift compression equations exist [23] for calculating the expected compression ratio and minimum pulse length for the case of an ideal velocity-tilted beam with arbitrary distribution passing through a perfectly neutralizing plasma. However, such emittance-dominated solutions do not include the finite-size gap effects, such as the reduction in tilt  $f$ , effective temperature increase, or increased chromatic aberration experienced by the head particles compared to the tail particles. The general derivation of the constant that takes into account the effective temperature imparted onto the beam by the finite-size gap is not provided here. The effective longitudinal temperature of the beam exiting the gap is intimately linked to the minimum pulse length when a nearly ideal waveform is employed, with smaller  $T_b$  associated with higher compression ratios and shorter pulse lengths. Deviations from the ideal slope by the experimental waveform also increase the effective temperature inferred by the measured pulse length. When such errors in the voltage waveform dominate the aberration due to initial  $T_b$ , the minimum pulse length is said to be waveform-dominated, instead of emittance-dominated. In reality, Eq. (18) is of limited value because the minimum achievable pulse length is actually a complex function of many realistic considerations, including partial neutralization effects.

### C. Dependence on initial pulse length and intended fractional tilt

Since the voltage waveform of the induction module imparts the axial velocity tilt to the beam, it is inextricably linked to the amount of current compression achieved at the focal plane. Assume that the ideal waveform  $V(t)$  can be accurately reproduced over the duration of the intended pulse length  $t_p$ , as in the “smooth” waveform. The two  $V(t)$  waveform parameters that can be adjusted by the experimenter are the intended pulse length  $t_p$  and the amount of desired fractional tilt  $f$ .

First, consider changes in  $V(t)$  due to  $t_p$ , while holding  $E_0 = 400$  keV and  $f = 0.5$  constant. The “smooth”

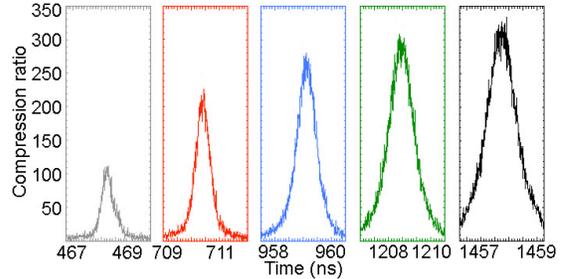


FIG. 15: (Color) Compression ratios  $I_b(t)/I_0$  in the laboratory frame at the focal planes using the color-coded “smooth” waveforms of Fig. 14 across the finite-size gap for  $T_b = 0.2$  eV,  $f = 0.5$ , and  $t_p = 100$  ns (gray),  $t_p = 200$  ns (red),  $t_p = 300$  ns (blue),  $t_p = 400$  ns (green), and  $t_p = 500$  ns (black).

waveforms for  $t_p = 100$  ns to 500 ns, in steps of 100 ns, are displayed in Fig. 14. All of the waveforms considered here are  $\pm 180$  kV symmetric, as opposed to the waveform in Fig. 1. The reason is that a plus-minus symmetric waveform takes the most advantage of the available voltage for a given limit, due to voltage hold-off considerations. The drift length  $L_d$  increases linearly with  $t_p$  for constant  $E_0$  and  $f$  [Eq. (6)], as does the amount of aberration [Eqs. (12) and (13)] and the minimum achievable pulse length [Eq. (18)]. The competing effect is the increasing amount of longitudinal compression, since the compression of longer initial  $t_p$  results in larger amounts of total current at the focal plane, assuming charge conservation [ $I^f/I_0 = (q^f/t_p^f)(q_0/t_p^0)^{-1} = t_p^0/t_p^f$  for  $q^f = q_0$ ]. However, the effect plateaus due to increased aberration associated with longer  $L_d$ . Therefore, careful assessment of the desired amount of compression compared to the desired minimum pulse length at focus and available plasma column for experiments is required.

The simulation results for current compression of an  $E_0 = 400$  keV and  $T_b = 0.2$  eV  $K^+$  ion beam using the color-coded “smooth” waveforms of Fig. 14 across the 3 cm gap are shown in Fig. 15. The actual initial  $t_p$  are longer than the prescribed lengths intended to undergo compression. The extra voltage in the “smooth” waveform acts on the extra initial  $t_p$  to increase the compression ratio, tilt  $f$ , and  $t_{fwhm}$  (slightly) achieved at the focal plane compared to the “sharp” waveform case. The compression dependence on initial pulse length at the focal plane is provided in Table II in terms of the compression ratio, full-width, half-maximum pulse length, drift length, and the spatial offset between the focal lengths for the finite-size and infinitely thin gaps ( $\Delta L_d$ ). The data in Table II correspond to the results in Fig. 15.

The compression ratio increases as  $\sim t_p^{0.8}$  for shorter initial pulse lengths, but as  $\sim t_p^{0.3}$  for longer initial pulse lengths. The minimum  $t_{fwhm}$  increases as  $\sim t_p^{0.3}$  for shorter initial pulse lengths, but as  $\sim t_p^{1.05}$  for longer initial pulse lengths, in agreement with the linear dependence of Eq. (18). Recall that Eq. (18) underestimates

TABLE II: Compression dependence on initial pulse length  $t_p$  for  $E_0 = 400$  keV,  $T_b = 0.2$  eV, and an intended  $f = 0.5$  using the “smooth” waveform across the 3 cm long gap.

$t_p$	$I_b^{max}/I_0$	$t_{fwhm}$	$L_d$ [Eq. (6)]	$\Delta L_d$
100 ns	120	0.5 ns	26.2 cm	+2.65 cm
200 ns	220	0.6 ns	52.5 cm	+1.45 cm
300 ns	280	0.7 ns	78.7 cm	+1.25 cm
400 ns	310	0.9 ns	104.9 cm	+1.15 cm
500 ns	325	1.2 ns	131.2 cm	+0.95 cm

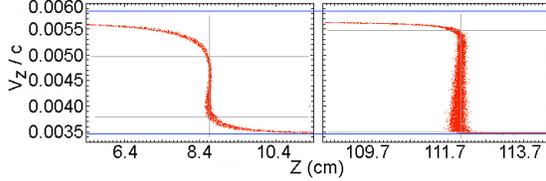


FIG. 16: (Color)  $\{z, v_z\}$  phase space near the focal planes for the  $t_p = 100$  ns (left) and  $t_p = 500$  ns (right) cases shown in Fig. 15 and Table II. Blue and gray horizontal lines demarcate the expected  $v_h$  and  $v_t$  for  $f = 0.5$ , and show the minimum  $v_h$  and maximum  $v_t$  achieved by the beam, respectively.

the pulse length at focus by an approximately constant 20% for  $t_p \geq 300$  ns, due to the 45% extra effective longitudinal temperature given to the beam by the gap effects. Although, as  $t_p$  decreases to 200 ns and 100 ns, the underestimation of  $t_{fwhm}$  by Eq. (18) increases to 36% and 62%, respectively, since the initial  $L_b$  and  $t_p$  each become comparable to the effective gap length and transit time, respectively. The failure of Eq. (18) for short  $t_p$  is expected, since its derivation assumed an infinitely thin gap relative to the initial  $L_b$ . Essentially, beam particles sample large amounts of the  $V(t)$  if the gap is not thin enough, resulting in a reduced effective  $f$  ( $v_h$  too large and  $v_t$  too small) that is a function of initial  $t_p$ . Although none of the simulations recover the intended  $f = 0.5$ , longer initial  $t_p$  achieve greater  $f$ , but at the cost of more longitudinal aberration from  $T_b$  over the greater drift lengths. Figure 16 illustrates both phenomena graphically. The actual  $f$  achieved for  $t_p = 100$  ns and  $t_p = 500$  ns are  $f \sim 0.25$  and  $f \sim 0.43$ , respectively. The compression ratio for the  $t_p = 300$  ns case is reduced to 280 (from 320 previously), and corresponds to the same percentage reduction in waveform voltage late in time ( $-225$  kV to  $-180$  kV).

The last column of Table II shows that, as the initial pulse length increases relative to the effective gap transit time, the spatial (and also temporal) offset between the focal lengths for the finite-size and infinitely thin gaps decreases ( $\sim t_p^{-0.6}$ ). Therefore, the origin of the offset mentioned earlier between the two gap cases lies in the quantitative ratios of  $L_b$  and  $t_p$  to the effective gap length and transit time, respectively. Another interpretation would be that the finite-size gap changes the resulting tilt  $f$  while decreasing the  $v_t$  more than increasing the

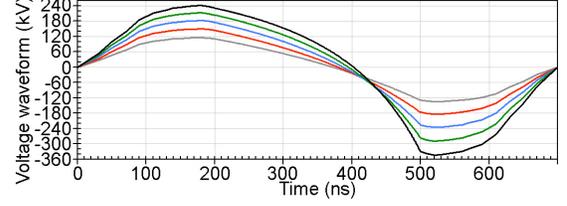


FIG. 17: (Color) “Smooth” voltage waveforms  $V(t)$  for  $E_0 = 400$  keV,  $t_p = 300$  ns, and  $f = 0.3$  (gray),  $f = 0.4$  (red),  $f = 0.5$  (blue),  $f = 0.6$  (green), and  $f = 0.7$  (black).

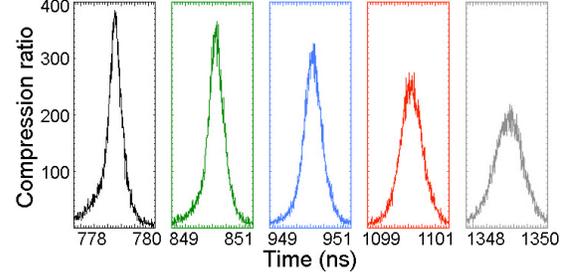


FIG. 18: (Color) Compression ratio  $I_b(t)/I_0$  comparison using the color-coded “smooth” waveforms of Fig. 17 across the finite-size gap in the laboratory frame at the focal planes for  $T_b = 0.2$  eV,  $t_p = 300$  ns, and  $f = 0.3$  (gray),  $f = 0.4$  (red),  $f = 0.5$  (blue),  $f = 0.6$  (green), and  $f = 0.7$  (black).

$v_h$ , and therefore  $L_d$  [refer to Eq. (3)] becomes larger compared to the case where the velocities are changed by the same amount.

Second, consider changes in  $V(t)$  due to the intended tilt  $f$ , while holding  $E_0 = 400$  keV and  $t_p = 300$  ns constant. The “smooth” waveforms for  $f = 0.3$  to  $f = 0.7$ , in steps of  $f = 0.1$ , are displayed in Fig. 17. Now none of the waveforms are  $\pm V^{max}$  kV symmetric, in order to capture the full voltage range for each of the  $f$ . The required time and drift length to the focal plane decrease as  $\frac{1}{f} + \frac{1}{2}$  and  $\frac{1}{f} - \frac{f}{4}$ , respectively, with increasing  $f$  for constant  $E_0$  and  $t_p$  [Eqs. (5) and (6)]. The amount of aberration [Eqs. (12) and (13)] and the minimum pulse length [Eq. (18)] decrease with increasing  $f$ , as well. Therefore, larger tilts are generally desired for increased levels of current compression and shorter pulse lengths. However, a careful assessment of the desired amount of compression compared to the increased focusing aberration, associated with the energy tilt during transverse compression to a coincident focal plane, is required.

The simulation results for current compression of an  $E_0 = 400$  keV and  $T_b = 0.2$  eV  $K^+$  ion beam using the color-coded “smooth” waveforms of Fig. 17 across the 3 cm gap are shown in Fig. 18. The actual initial  $t_p$  are longer than the prescribed  $t_p = 300$  ns intended to undergo compression. The compression dependence on the intended fractional tilt  $f$  at the focal plane is

TABLE III: Compression dependence on the intended tilt  $f$  for  $E_0 = 400$  keV,  $T_b = 0.2$  eV, and  $t_p = 300$  ns using the “smooth” waveform across the 3 cm long gap.

$f$	$I_b^{max}/I_0$	$t_{fwhm}$	$L_d$ [Eq. (6)]	$\Delta L_d$
0.3	210	1.4 ns	136.8 cm	+1.00 cm
0.4	260	1.0 ns	100.7 cm	+1.25 cm
0.5	320	0.7 ns	78.7 cm	+1.25 cm
0.6	360	0.6 ns	63.7 cm	+1.25 cm
0.7	380	0.5 ns	52.6 cm	+1.35 cm

provided in Table III in terms of the compression ratio, full-width, half-maximum pulse length, drift length, and the spatial offset between the focal lengths for the finite-size and infinitely thin gap cases ( $\Delta L_d$ ). The data in Table III correspond to the results in Fig. 18.

The compression ratio increases as  $\sim f^{0.82}$  for smaller intended  $f$  ( $0.3 \leq f < 0.5$ ), but as  $\sim f^{0.51}$  for larger intended  $f$  ( $0.5 \leq f < 0.7$ ). The minimum  $t_{fwhm}$  decreases with increasing  $f$  as  $\sim f^{-1.23}$ , in agreement with the  $\sim f^{-1.25}$  dependence in Eq. (18). Although, the  $t_{fwhm}$  from Eq. (18) maintains its 20% underestimation at focus as a function of  $f$ , since the ratios of the initial  $L_b$  and  $t_p$  to the effective gap length and transit time, respectively, remain constant. The constant offset of Eq. (18) offers validation that the discrepancy is solely due to the relative size of the mentioned geometric parameters, and not the intended tilt  $f$ . As before, the intended fractional tilt is not achieved in any of the cases presented in Table III. The resulting relative decrease is approximately 20% for  $t_p = 300$  ns and independent of  $f$ . Recall that the compression ratio reduction and full-width, half-maximum pulse length increase due to the gap were also reported to be 20%. Again, smaller tilts  $f$  suffer more aberration from  $T_b$  due to the greater  $L_d$  required.

The last column of Table III shows that the spatial (and also temporal) offset between the focal lengths for the finite-size and infinitely thin gap cases is approximately independent (or very weakly dependent on) of  $f$ , since the initial bunch and pulse lengths relative to the effective gap length and transit time across the gap, respectively, are approximately constant. In addition, the required time and drift length to the focal plane decrease approximately with  $\sim f^{-0.81}$  and  $\sim f^{-1.12}$  dependence, respectively, in agreement with Eqs. (5) and (6).

The results presented in this subsection indicate that an optimum drift length exists, for a given set of beam parameters, that balances the larger compression ratios achieved by longer initial  $t_p$  and larger  $f$  with the increased  $t_{fwhm}$  values of the former and decreased  $t_{fwhm}$  values of the latter. Longer initial  $t_p$  are shown to increase  $L_d$ , as well as increase aberration, and shorter initial  $t_p$  are shown to achieve smaller  $f$  due to the finite-size gap. Also, larger tilts are shown to decrease  $L_d$  and aberration, but will adversely affect the transverse aberration during final focus. The amount of tilt achieved in the laboratory is limited by the magnetic flux of the induction

module and voltage hold-off considerations in the gap.

#### D. Dependence on energy and thermal distribution

The last topic covered in this Section is the dependence of current compression on the ion beam kinetic energy and distribution function. The derivation of the ideal  $V(t)$  assumed a particular initial (and constant) beam energy  $E_0$ . Since the  $V(t)$  slope is only ideal for one particular  $E_0$ , slight energy differences cause the beam to focus to different axial locations, with lower compression ratios and longer pulse lengths. Also, the longitudinal distribution is expected to affect compression, since aberration causes smearing of the focus in time and space. Then, the resulting current profile is a direct consequence of the distribution of particle energies, and both the average  $E_0$  [or  $E_0(t)$ ] and the distribution play a role. Various pulse shapes may therefore be realized at the target.

In the laboratory, the accuracy of  $E_0$  is approximately  $\pm 5\%$ . In order to maximize the reliability of the longitudinal focusing capability, the shot-to-shot variation in directed beam energy and imposed waveform must be minimized. Also, the  $E_0(t)$  over the microseconds of its long initial pulse length might generally not be constant, since it depends on the high-power diode technology employed. In practice, the injected  $E_0(t)$  may fluctuate on fast time scales (contributing to longitudinal emittance), as well as drift its mean energy by as much as  $\pm 10\%$  over a  $t_p = 6 - 10 \mu\text{s}$  pulse, or as much as  $\pm 1 - 2\%$  over a window of  $\sim 300$  ns. In order to quantify the effects on compression from these two types of energy variations, a set of simulations are carried out.

First, recall the compression simulation across the finite-size gap using a “smooth” waveform, with the parameters  $E_0 = 400$  keV,  $t_p = 300$  ns, and  $f = 0.5$ , and an initialized Maxwellian temperature of  $T_b = 0.2$  eV; the results are in Fig. 10, and the focal plane is located at  $z = +59.5$  cm and  $t = 959$  ns. The simulation is repeated four times, except the constant initial beam energy is  $E_0 = 380$  keV ( $-5\%$ ),  $390$  keV ( $-2.5\%$ ),  $410$  keV ( $+2.5\%$ ), and  $420$  keV ( $+5\%$ ), in order to represent the  $\pm 5\%$  accuracy of the  $E_0$  in experiments.

The current compression profiles through the originally intended plane for the four cases are shown in Fig. 19. The more energetic beams arrive first, followed by the less energetic beams in order. The two beam cases with larger  $v_0$  have not reached their focal planes at this  $z$  because their  $L_d$  are longer. The opposite is true for the charge bunches with smaller  $v_0$ , and those two cases are already beyond their focal planes at this  $z$ .

In order to directly compare the amount of compression achieved by the different  $E_0$  beams using the waveform intended for an  $E_0 = 400$  keV beam, the current profiles through their respective focal planes are plotted as a function of absolute time on a linear scale in Fig. 20; the five plots are color-coded to match those in Fig. 19. The compression dependence at the focal plane is

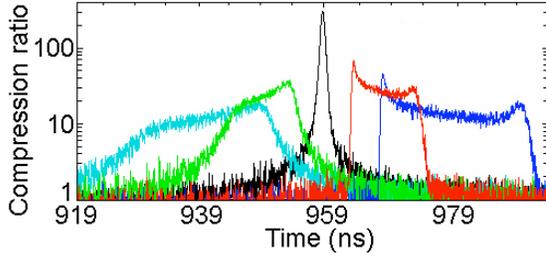


FIG. 19: (Color) Compression ratio  $I_b(t)/I_0$  (Log scale) comparison of  $\pm 5\%$  constant  $E_0$  variations using the “smooth” waveform across the finite-size gap and  $T_b = 0.2$  eV beams at  $z = +59.5$  cm in the laboratory frame for  $E_0 = 420$  keV (light blue),  $E_0 = 410$  keV (green),  $E_0 = 400$  keV (black),  $E_0 = 390$  keV (red), and  $E_0 = 380$  keV (dark blue).

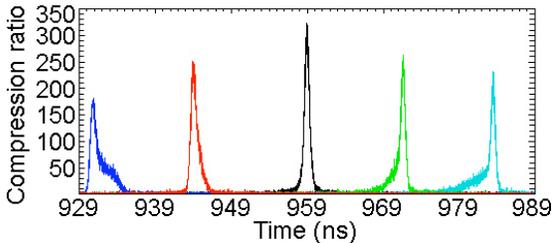


FIG. 20: (Color) Compression ratio  $I_b(t)/I_0$  comparison in the laboratory frame for  $\pm 5\%$  constant  $E_0$  variations using the “smooth” waveform across the finite-size gap and  $T_b = 0.2$  eV beams for  $E_0 = 420$  keV (light blue) at  $z = +65.0$  cm,  $E_0 = 410$  keV (green) at  $z = +62.3$  cm,  $E_0 = 400$  keV (black) at  $z = +59.5$  cm,  $E_0 = 390$  keV (red) at  $z = +56.4$  cm, and  $E_0 = 380$  keV (dark blue) at  $z = +53.6$  cm. The plots are color-coded to the profiles of the same color in Fig. 19.

provided in Table IV in terms of the compression ratio, full-width, half-maximum pulse length, total time to focus, and the location of the focal plane in the PIC axial coordinates. The data in Table IV correspond to the results in Fig. 20.

Small ( $\pm 2.5 - 5\%$ ) discrepancies in  $E_0$  from the intended beam energy for the particular  $V(t)$  result in a range of approximately 20–40% relative decrease, respectively, in the amount of compression measured at the different focal planes. Higher energies achieve shorter  $t_{fwhm}$  at longer  $L_d$  and later in time. However, the  $t_{fwhm}$  value does not reflect the significant current pedestals formed by the energy inaccuracy, which are particularly virulent for the  $\pm 5\%$  cases in Fig. 20. Changes in beam energy by  $\pm 10$  keV ( $\pm 2.5\%$ ) result in an average change of  $\pm 2.8$  cm in the focal plane location.

A particular  $V(t)$  slope results in optimum compression only for a particular  $E_0$  at the intended focal plane. Beam energy scans to align a diagnostic with a peak compression result, while holding  $V(t)$  fixed, do not unambiguously locate the true optimum compression achievable for the waveform under consideration, as quanti-

TABLE IV: Compression dependence on initial  $E_0$  inaccuracy over a  $\pm 5\%$  range with  $T_b = 0.2$  eV for  $E_0 = 400$  keV,  $t_p = 300$  ns, and  $f = 0.5$  using the “smooth” waveform across the 3 cm long gap.

$E_0$	$I_b^{max}/I_0$	$t_{fwhm}$	$t^{foc}$	$z^{foc}$
380 keV	180	0.9 ns	930.9 ns	+53.6 cm
390 keV	250	0.8 ns	944.1 ns	+56.4 cm
400 keV	320	0.7 ns	959.0 ns	+59.5 cm
410 keV	260	0.7 ns	971.8 ns	+62.3 cm
420 keV	230	0.6 ns	983.7 ns	+65.0 cm

tatively shown in Fig. 20 and Table IV. Discernment of the actual optimum compression due to a particular waveform is possible by first fixing both  $E_0$  and  $V(t)$  and conducting an axial scan of the profiles in the focal plane vicinity with a movable diagnostic. Once a set of ratios  $I_b(t)/I_0$  at multiple axial locations before and after the focal plane is measured, such as many of those presented throughout this paper, the repetition of such a set of measurements for various  $E_0$  with  $V(t)$  fixed will result in the conclusive determination of the achievable optimum compression for the given  $V(t)$ . The peak compression profiles from each set of measurements for various  $E_0$  would look similar to Fig. 20 when plotted together. Without an axial scan by the diagnostic for a range of  $E_0$ , any of the measured maximum compression ratios portrayed in Fig. 20 may be mistaken for the “optimum” compression ratio when, in fact, only one of them may be so called (the black one).

Second, the  $E_0$  of the injected beam might not be generally uniform. In practice, the beam energy in experiment may fluctuate on fast time scales (contributing to emittance), as well as drift its mean energy by as much as  $\pm 1 - 2\%$  over a window of  $\sim 300$  ns. In order to quantify the effects of an average energy drift as the beam enters the gap, two additional similar simulations are carried out. The first allows the  $E_0(t)$  of the 400 keV beam to rise linearly with time over the pertinent  $t_p = 300$  ns to  $E_0 = 408$  keV (+2%); the second allows the  $E_0(t)$  of the same beam to sink linearly with time over the pertinent  $t_p = 300$  ns to  $E_0 = 392$  keV (−2%).

In order to compare the amount of compression achieved by the beams with increasing and decreasing  $E_0(t)$  using the waveform intended for a  $E_0 = 400$  keV beam, the current profiles through their respective focal planes are plotted as a function of absolute time on a linear scale in Fig. 21. The focal plane of the original  $E_0 = 400$  keV simulation is located at  $z = +59.5$  cm and  $t = 959$  ns. Contrary to the previous simulation, the slightly more energetic beam arrives at its focal plane first, followed by the nominal and slightly less energetic beams, in order. The compression dependence at the focal plane on initial  $E_0$  with linear increase or decrease by  $\pm 2\%$  over the  $t_p = 300$  ns window is provided in Table V in terms of the compression ratio, full-width, half-maximum pulse length, total time to focus, and the

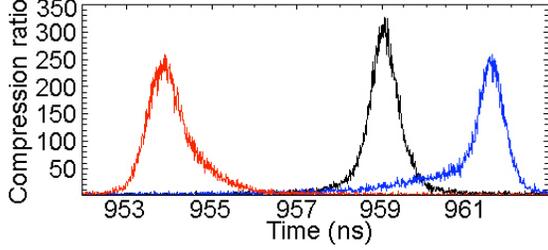


FIG. 21: (Color) Compression ratio  $I_b(t)/I_0$  comparison in the laboratory frame of initial  $E_0$  with linear increase or decrease by  $\pm 2\%$  over the pertinent  $t_b = 300$  ns, using the “smooth” waveform across the finite-size gap, for  $T_b = 0.2$  eV beams with rising  $E_0(t) = 400 - 408$  keV (red) at  $z = +59.3$  cm, constant  $E_0(t) = 400$  keV (black) at  $z = +59.5$  cm, and sinking  $E_0(t) = 400 - 392$  keV (dark blue) at  $z = +59.3$  cm.

TABLE V: Compression dependence on initial linear increase or decrease in  $E_0(t)$  by  $\pm 2\%$  with  $T_b = 0.2$  eV for  $E_0 = 400$  keV,  $t_p = 300$  ns, and  $f = 0.5$  using the “smooth” waveform across the 3 cm long gap.

$E_0$	$I_b^{max}/I_0$	$t_{fwhm}$	$t^{Joc}$	$z^{Joc}$
400 – 392 keV	250	0.8 ns	961.5 ns	+59.3 cm
400 keV	320	0.7 ns	959.0 ns	+59.5 cm
400 – 408 keV	250	0.8 ns	953.9 ns	+59.3 cm

location of the focal plane in the PIC axial coordinates. The data in Table V correspond to the results in Fig. 21.

Small ( $\pm 2\%$ ) increases or decreases in  $E_0(t)$  from the intended energy over the  $t_p = 300$  ns pulse length for the particular  $V(t)$  result in an approximate 22% relative decrease in the amount of compression. Both types of initial energy change achieve longer  $t_{fwhm}$  at a focal plane upstream of the nominal case, for the parameters considered here; although, the values of  $t_{fwhm}$  do not reflect the significant pedestals formed by the energy drifts, which are particularly prevalent in both cases in Fig. 21. Contrary to intuition, both types of temporal change in  $E_0(t)$  result in the formation of a focal plane at the same axial location, approximately 0.2 cm upstream of the nominal location, for the parameters considered here. The reason for the departure from the expected, such as the shorter (longer) drift length and time to focus for the faster (slower) beam, is that the linear temporal increase (decrease) in  $E_0(t)$  is effectively a decompressing (compressing) initial velocity tilt. Therefore, the beam whose energy increases (decreases) as a function of time entering the gap acquires a slightly larger (smaller) total tilt than nominal. Consequently, the relative  $L_d$  of the increasing (decreasing) energy case is slightly shorter (longer) than intended. In both cases, the peak compression ratio is relatively decreased compared to the beam with the proper  $E_0$  for the  $V(t)$ .

Unintentional experimental  $E_0(t)$  increases or decreases, whether constant in time or not, will not reach

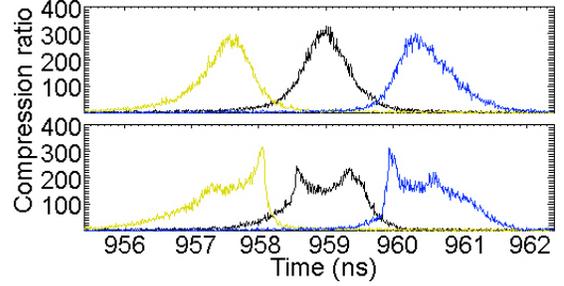


FIG. 22: (Color) Compression ratio  $I_b(t)/I_0$  comparison for the “smooth” waveform across the finite-size gap in the laboratory frame at  $z = +59.3$  cm (yellow), at the focal plane  $z = +59.5$  cm (black), and at  $z = +59.7$  cm (blue) for beams initialized with a  $T_b = 0.2$  eV Maxwellian (top profiles) and  $T_b = 0.6$  eV Waterbag distribution (bottom profiles).

the optimum compression achievable compared to the appropriate constant  $E_0$  case for the specific  $V(t)$ . This is quantitatively illustrated in Figs. 20 and 21 and Tables IV and V. In summary, if a beam enters the gap with an  $E_0(t)$  too high/low (or increasing/decreasing in time) by a few percent, one of the suboptimal “maximum” compression ratios may be measured and mistaken for the actual optimum ratio. Beams with constant  $E_0$  a few percent larger (smaller) than the appropriate  $E_0$ , or with an  $E_0(t)$  profile rising (sinking) by a few percent over the initial  $t_p$ , result in the deformation of the vertical  $\{z, v_z\}$  phase space at focus into one slightly curved forward (backward), rather than entirely vertical. Both types of change reduce compression by smearing the focal plane in a manner similar to aberration.

The type of beam distribution that characterizes the longitudinal temperature affects the shape of the current profiles, and therefore the associated compression. The original simulation is revisited one last time in order to discern the effect on longitudinal focus (at  $z = +59.5$  cm and  $t = 959$  ns) when the  $T_b = 0.2$  eV Maxwellian distribution is changed to a  $T_b = 0.6$  eV Waterbag distribution. Recall that the Waterbag distribution is a uniform-density and equally-populated distribution between  $v_0 - v_{th}$  and  $v_0 + v_{th}$ , and the two distributions satisfy  $v_{th}^W = \sqrt{3} v_{th}^M$  for  $T_M = T_W$ . However, in order to equally compare the shape of the two distributions, the width of the Waterbag distribution must be equal to the full  $3 v_{th}^M$  ( $3 \sigma = 99.73\%$ ) Maxwellian distribution, so  $v_{th}^W = 3 v_{th}^M$  and  $T_W = 3 T_M$  are employed.

The current profiles for the Maxwellian and Waterbag distributions near the shared focal plane ( $z = +59.5$  cm) are plotted as a function of absolute time on a linear scale in Fig. 22. At  $t = 959$  ns, the Maxwellian current profile peaks at a compression ratio of 320, whereas the Waterbag current profile is near a local minimum compression ratio of 150. Compression ratios closer to the Maxwellian maximum for the Waterbag case (300 – 320) are found just upstream and downstream from the in-

tended focal plane at later and earlier times, respectively. The  $t_{fwhm}$  are similar, but the Maxwellian case maintains higher compression ratios near the profiles' centers due to the increased velocity space population densities near the desired  $v_z$  values for the  $V(t)$  compared to the Waterbag case, whose velocity space population densities are equidistant about the same desired  $v_z$  values.

The bell-shaped normal distribution in the Maxwellian case achieves more compression and therefore shorter values of  $t_{fwhm}$  times. The bell shapes in the Maxwellian case are replaced with shapes approximating squares in the Waterbag case. The sharp peaks in current late (early) in time for individual profiles upstream (downstream) of the intended focus are due to the sharp velocity space boundaries of the Waterbag distribution; the more diffuse Maxwellian case does not have the same features. The sharp Waterbag velocity space boundaries for the faster tail particles contribute to relatively larger peaks in current because of the decreased levels of aberration suffered by the tail compared to the head. Therefore, the relatively increased current peaks arrive later (earlier) in time for profiles upstream (downstream) of focus. In practice, intense beam distributions are closer to Maxwellian because of their creation from an emitter maintained at a certain temperature in the NDCX device. However, the blue Waterbag profile in Fig. 22 suggests that, if an ion beam with a Waterbag distribution could be used for compression experiments, pre-heat of targets could be reduced because the pre-pulse current pedestal is lower compared to the Maxwellian analog, and the elapsed time required by the Waterbag profile to increase from low to peak current is shorter than the same required by the Maxwellian distribution.

#### IV. SIMULTANEOUS TRANSVERSE AND LONGITUDINAL ION BEAM FOCUSING

At the present time, the compression of ion beams in the laboratory has been separately demonstrated in the transverse and longitudinal directions. However, simultaneous focusing to a common focal plane is desired in order to maximize the intensity on the target [18]. The goal for upcoming experiments is to demonstrate the feasibility and study the physical limitations of simultaneous transverse and longitudinal compression of an intense charge bunch [7, 15, 24].

##### A. Transverse defocusing effect

As mentioned in Section III.A, the process of imposing an axial velocity tilt for the purpose of longitudinal compression contributes a time-dependent net divergence to the otherwise radially converging trajectories of the ions [18, 21], as well as imparts velocity spread akin to an effective longitudinal temperature on an otherwise initially cold beam. The time-dependent nature of the  $V(t)$ ,

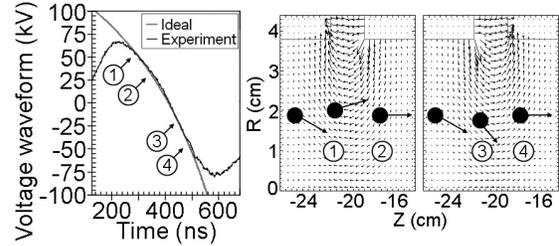


FIG. 23: Illustration of the radial defocusing effect of the acceleration gap. For  $dV(t)/dt < 0$ , particles crossing the gap early in time [when  $V(t) > 0$ , shown as 1 and 2] sample more integrated  $+E_r$  at the entrance compared to the exit, whereas particles crossing the gap late in time [when  $V(t) < 0$ , shown as 3 and 4] sample more integrated  $+E_r$  at the exit compared to the entrance. In the center and right frames, electric field vectors are plotted and the black arrows indicating particle velocity vectors are exaggerated.

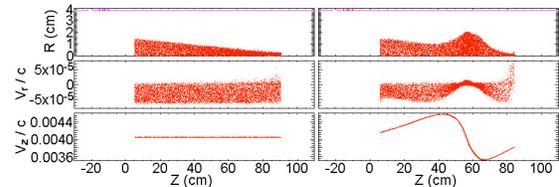


FIG. 24: (Color) Beam phase space comparison between transverse focusing without (left) and with (right) an axial velocity tilt at  $t = 1000$  ns, shown as particle plots in  $\{r, z\}$  (top),  $\{z, v_r\}$  (middle), and  $\{z, v_z\}$  (bottom) coordinates. The radial defocusing effect imparts excess divergence to the longitudinally compressing portion of the beam in a time-dependent manner.

combined with the sizeable transit time of the ion particles across the gap, imply an imbalance of integrated  $E_r(r, z, t)$  experienced by each particle and provides a time-dependent radial defocusing force to both the head and tail of the beam, as illustrated in Fig. 23.

A  $2D \{r, z\}$  PIC simulation of transverse focusing without an axial velocity tilt is compared to the same with an applied axial velocity tilt. An  $E_0 = 300$  keV  $K^+$  beam with an initial radius  $r_b = 2$  cm and  $I_0 = 18$  mA of beam current is initialized with a Maxwellian  $T_b = 0.2$  eV and a convergence angle of  $\Delta\theta_r = -15.4$  mrad at the injection plane  $z = -30$  cm, just upstream of the gap. The initial  $t_p = 700$  ns and the  $V(t)$  waveform imposes an approximate  $f = 0.1$  tilt to the beam. In this case, the background plasma is sufficiently dense and cold to ensure good neutralization throughout the drift length.

Particle phase space plots with and without the velocity tilt are displayed in Fig. 24 after the beam passes the acceleration gap and enters the plasma ( $t = 1000$  ns). The difference in trajectories due to acceleration gap dynamics is clear. A hump-shape in  $\{r, z\}$  space around the region of the axially compressing charge bunch ap-

pears due to the radial defocusing effect, and the  $r_b(t)$  at focus is increased considerably ( $\sim 2$  cm) compared to the case without a tilt ( $\sim 0.2$  cm). The consequence of the defocusing effect on current density compression is striking, because of the  $r_b(t)^{-2}$  dependence on  $J_z$ . Early longitudinal compression experiments substantiated the existence of the effect [11], and agreed with simulations.

The effective transverse (in addition to the longitudinal) temperature of the charge bunch changes relative to the cold beam case, and is manifest in the time-dependent radial velocity spread of the beam as it exits the gap. The time-dependent range of the radial velocity spreads will overlap in the axial coordinate near the longitudinal focal plane and have an effective temperature, and associated aberration, different than the  $T_b$  in the case without a velocity tilt. The two types of coupled transverse and longitudinal focusing and effective temperature increase are dependent upon the gap geometry, voltage waveform, and beam parameters, such as axial velocity, radius, and convergence angle.

### B. Final-focus solenoid for transverse focusing

One method for “re-focusing” the defocused beam in order to achieve simultaneous compression to a sub-mm  $r_b$  at the focal plane involves the use of a strong final-focus solenoid [7, 18]. The use of a final-focus solenoid near the end of the drift length controls the effective focal length of the transverse compression, and therefore helps minimize the amount of plasma required throughout the system, in addition to decreasing the amount of aberration compared to a longer transverse focal length. A strong axial magnetic field has been shown to reduce magnetic filamentation, particularly at high beam densities, since plasma electrons are magnetized and constrained to move along field lines [25]. Two other methods under active research are the “over-focusing” technique [18], which only offsets the defocusing effect in an average way, and corrective time-dependent magnetic focusing, the technology for which is currently unavailable.

An energy-tilted beam entering a final-focus solenoid results in aberration of the transverse focal plane [7, 24]. For a static  $\mathbf{B}^{sol}(r, z)$ , the lower-energy head (higher-energy tail) of the tilted beam transversely focuses earlier (later) in space and time; the axial placement of the solenoid must be precisely positioned in order to ensure the optimal amount of simultaneous compression. A smaller tilt  $f$  alleviates some of the transverse aberration, but at the cost of reducing the longitudinal compression. The  $\mathbf{B}$  field of a finite length and radius solenoid is modeled in the LSP code by using a power-series expansion of the radial coordinate, which involves only the on-axis  $r = 0$  field and its derivatives [26]. The PIC simulations employ a strong 150 kG final-focus solenoid of length  $l^{sol} = 20$  cm and radius  $r^{sol} = 3.8$  cm, centered at  $z = +52.6$  cm, as illustrated in Fig. 25. In general, the location of the transverse focal plane (and its aberration)

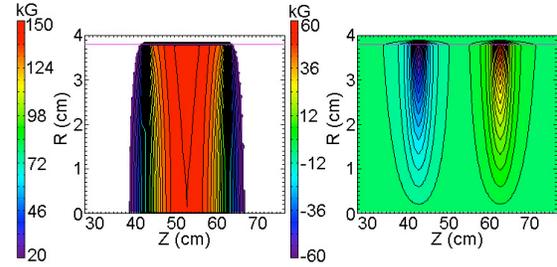


FIG. 25: (Color)  $\{r, z\}$  isocontours of axial  $B_z$  (left) and radial  $B_r$  (right) field magnitudes from a 150 kG solenoid of length  $l^{sol} = 20$  cm and radius  $r^{sol} = 3.8$  cm, centered at  $z = +52.6$  cm.

tion) depends on the length and strength of the solenoid, as well as the  $r_b(t)$  and velocity space distribution of the beam as it enters the solenoid.

In order to quantify the effects arising from the solenoid rather than those from the gap, the case of an ideally-tilted beam using the “sharp” waveform across an infinitely-thin gap, with initial parameters  $E_0 = 400$  keV,  $t_p = 300$  ns,  $f = 0.5$ , and Maxwellian  $T_b = 0.2$  eV, is revisited with the addition of the 150 kG solenoid. The original simulation resulted in a compression ratio of  $I_b^{max}/I_0 = 400$  with  $t_{fwhm} = 0.6$  ns at the focal plane  $z = +58.25$  cm at time  $t = 950$  ns. Here,  $|B_z| \sim 140$  kG at the intended focal plane. The beams are given initial radii of either  $r_b = 2$  cm or  $r_b = 1$  cm at  $z = -30$  cm, without convergence angles, and an initial current of 80 mA, which approximately represent the peak parameters available in the NDCX device. The plasma is assumed to be sufficiently dense and cold in order to provide neutralization of the beam throughout the drift length.

The less energetic head of the compressing charge bunch arrives at the final-focus solenoid first. Strong  $-B_r(r, z)$  fields are encountered, which rotate the beam via the Lorentz force,  $-F_\theta = +q[(+v_z) \times (-B_r)] = -m_i (dv/dt)_\theta$ . As found in the acceleration gap, the transverse and longitudinal dynamics are coupled, since the  $+v_z$  particle motion increases the  $-v_\theta$  rotation and leads to radial focusing,  $-F_r = +q[(-v_\theta) \times (+B_z)] = -m_i (dv/dt)_r$ . In addition, the  $-v_\theta$  is also the cause of axial deceleration via  $-F_z = +q[(-v_\theta) \times (-B_r)] = -m_i (dv/dt)_z$ , a second order effect. Beam particles at larger radii entering the solenoid encounter stronger  $-B_r(r, z)$  fields and acquire more  $-v_\theta$ , and subsequently more  $-v_r$  focusing (and  $-v_z$  deceleration), than those closer to the axis. All of the aforementioned velocities are functions of space and time due to the specific  $\mathbf{B}^{sol}(r, z)$ . However, beams with larger constant  $r_b$  suffer increased aberration in both focal planes due to the stronger integrated  $-B_r(r, z)$  encountered.

In addition to the cases involving beams of constant current density with initial radii of either  $r_b = 2$  cm or  $r_b = 1$  cm over the initial  $t_p = 300$  ns, two cases of radially-constant but temporally decreasing current den-

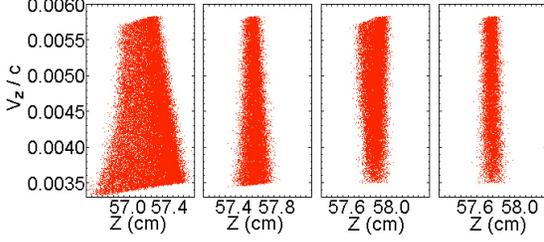


FIG. 26: (Color)  $\{z, v_z\}$  beam phase space plots for the constant  $r_b = 2$  cm (left), constant  $r_b = 1$  cm (middle left), decreasing  $J_z$  with linearly increasing  $r_b$  from  $r_b = 0.1$  to 2 cm (middle right), and decreasing  $J_z(t)$  with linearly increasing  $r_b(t)$  from  $r_b = 0.1$  to 1 cm (right) cases near the simultaneous focal planes  $z = +57.1$  cm at  $t = 946.9$  ns,  $z = +57.6$  cm at  $t = 949.3$  ns,  $z = +57.85$  cm at  $t = 951.0$  ns, and  $z = +57.85$  cm at  $t = 950.7$  ns, respectively.

sity  $[J_z(t) \sim r_b(t)^{-2}]$  with linearly increasing  $r_b(t)$  from  $r_b = 0.1$  cm to  $r_b = 2$  or 1 cm over the initial pulse length are considered. The  $I_0$  through the  $z = -30$  cm plane is 80 mA in all cases. For the non-constant  $J_z(t)$  cases under consideration, the optimum positioning of the solenoid is moved by  $\Delta z = +4$  cm to  $z = +56.6$  cm.

The reasoning behind the investigation of the cases involving a decreasing initial  $J_z(t)$  with linearly increasing initial  $r_b(t)$  is as follows. Slower head particles will normally transversely focus earlier than faster tail particles, contributing to transverse focusing aberration approximately proportional to  $r$  for a constant  $r_b$ . In order for the slower (faster) charge bunch head (tail) to transversely focus in a *longer* (*shorter*) axial distance and amount of time, they must enter the weaker (stronger)  $-B_r(r, z)$  fields at *smaller* (*larger*) radii, and thereby *decrease* (*increase*) the relative amount of  $-v_\theta$  rotation and radial focusing force  $-F_r$  they experience. Since the velocity tilt is nearly linear, and  $-B_r$  increases approximately linearly with  $r$  for  $r < r^{sol}$ , a charge bunch whose  $r_b(t)$  increases linearly from head to tail along the pulse length as it enters a final-focus solenoid minimizes the associated transverse focusing aberration.

The  $\{z, v_z\}$  beam phase space for the four cases are shown in Fig. 26 at their respective focal planes. The original longitudinal focal plane was at  $z = +58.25$  cm without the solenoid, about 0.4 – 1.15 cm downstream of the focal planes in the cases presented here (due to the net  $-v_z$  second-order effects). Beams with smaller radii suffer less simultaneous focusing aberration within the solenoid, and slower particles acquire an increased proportion of aberration for cases involving constant  $r_b$  (as in the longitudinal-only focusing cases). Interestingly, faster tail particles receive more longitudinal aberration in the case involving a linearly increasing  $r_b(t)$  to 2 cm due to the increased  $-B_r$  they encounter, whereas the nominal longitudinal compression results are recovered in the case involving a linearly increasing  $r_b$  to 1 cm.

When the finite-size gap effects are included, the exit-

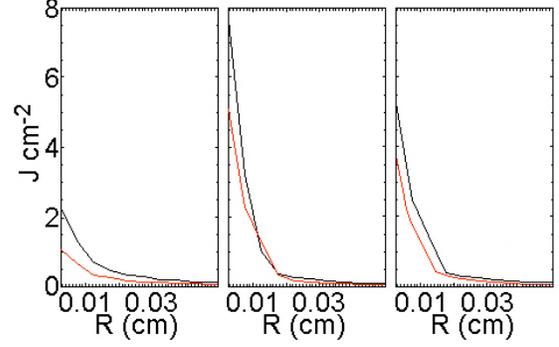


FIG. 27: (Color) Radial profiles of cumulative energy deposition  $E_{dep}(r)$  using a 150 kG solenoid and constant  $J_z$  (left), decreasing  $J_z(t)$  with linearly increasing  $r_b(t)$  (middle), and half-decreasing and half-increasing  $J_z(t)$  with linearly half-increasing  $r_b(t)$  and linearly half-decreasing  $r_b(t)$  (right) profiles for the cases involving  $r_b = 1$  cm (black) and  $r_b = 2$  cm (red) at the respective focal planes given in Fig. 26.

ing  $r_b(t)$  profile can be approximated as having a linear increase (decrease) over the first (second) half of the initial  $t_p$ , due to the transverse defocusing effect [refer to Fig. 24]. Such a triangular (or, parabolic because of the velocity tilt) pulse shape is simulated with linearly increasing  $r_b(t)$  from  $r_b = 0.1$  cm to  $r_b = 2$  cm or 1 cm over the first half and linearly decreasing  $r_b(t)$  from  $r_b = 2$  cm or 1 cm to  $r_b = 0.1$  cm over the second half duration of the initial  $t_p$  [with radially-constant  $J_z(t) \sim r_b(t)^{-2}$  variation to ensure  $I_0 = 80$  mA]. Since the first half of the pulse has the desirable linear  $r_b(t)$  increase and the second half will suffer less relative aberration due to the decreasing  $r_b(t)$ , the triangular case is expected to return intermediate compression results between the constant and linearly increasing  $r_b(t)$  cases.

Radial profiles of cumulative energy deposition  $E_{dep}(r)$  for the six cases under discussion are displayed in Fig. 27. The case shown in the middle frame for the linearly increasing  $r_b(t)$  from  $r_b = 0.1$  cm to  $r_b = 1$  cm recovers the original current compression ratio of 400 with a  $t_{fwhm} = 0.6$  ns and radius  $(1/e)$   $r_b^{foc} = 80$   $\mu$ m, yielding a peak on-axis  $E_{dep}^{peak} = 7.7$   $\text{J cm}^{-2}$  and approximate intensity 8  $\text{GW cm}^{-2}$ . Therefore, this  $r_b(t)$  profile entering the final-focus solenoid is better for minimizing aberrations. The results for all of the cases are listed in Table VI in terms of the compression ratio, full-width, half-maximum pulse length, peak on-axis  $E_{dep}$ , and approximate minimum simultaneous  $r_b^{foc}(1/e)$ . Note that the triangular cases, which more closely represent present experimental conditions, result in better compression than the average of the other two types of cases considered, because of the reduced  $r_b(t)$  and experienced  $-B_r(r, z)$  later in the pulse compared to the constant  $r_b$  cases.

In summary, the  $r_b(t)$  profile produced by the transverse defocusing effect is beneficial for reducing the aber-

TABLE VI: Compression dependence on initial  $r_b(t)$  profile using a 150 kG solenoid.

Initial $r_b(t)$	$I_b^{max}/I_0$	$t_{fwhm}$	$E_{dep}^{peak}$	$r_b^{foc}$ (1/e)
2 cm, constant	100	2.7 ns	1.1 J cm <sup>-2</sup>	110 $\mu$ m
1 cm, constant	310	0.8 ns	2.3 J cm <sup>-2</sup>	110 $\mu$ m
2 cm, triangular	275	0.8 ns	3.8 J cm <sup>-2</sup>	100 $\mu$ m
1 cm, triangular	375	0.7 ns	5.3 J cm <sup>-2</sup>	100 $\mu$ m
2 cm, linear increase	290	1.0 ns	5.0 J cm <sup>-2</sup>	100 $\mu$ m
1 cm, linear increase	400	0.6 ns	7.7 J cm <sup>-2</sup>	80 $\mu$ m

ration normally imposed on a beam with constant  $r_b(t)$  entering a final-focus solenoid. Further laboratory improvements for simultaneous focusing using a final-focus solenoid could use time-dependent magnetic focusing, in tandem with the calculated defocusing effect, in order to ensure a beam with a linearly increasing  $r_b(t)$  exits the gap, rather than the approximately triangular (or, parabolic) profile presently available. Alternatively, a change in gap conducting boundary geometry that decreases the  $E_r$  imbalance early in time but exacerbates the defocusing late in time, can result in a linearly increasing  $r_b(t)$  profile, as well. Lastly, if the focal plane is chosen to be downstream of the solenoid (for shorter and/or weaker solenoids), the  $-v_\theta$  velocities approach their original values upon exiting the solenoid due to the  $+B_r(r, z)$  fields. However, due to the inward radial movement within the solenoid, the beam will have a smaller  $r_b(z, t)$  as it exits and not sample a balanced amount of  $+B_r(r, z)$  compared to the  $-B_r(r, z)$  at the entrance. After the beam leaves the region of strong  $B_z$ , and  $-v_\theta$  decreases in magnitude, the net radial converging trajectory remains and transversely propagates the beam to its simultaneous focal plane.

## V. SUMMARY AND CONCLUSIONS

In this paper, the derivation of an ideal velocity tilt, and the voltage waveform  $V(t)$  that produces it, was presented for a cold ion beam encountering an infinitely thin acceleration gap and subsequently undergoing longitudinal compression (Sec. II). Under such idealized circumstances, no theoretical finite upper bound on the bunch compression exists. However, such a perfectly compressed beam can not be realized in experiments, since all beams have finite temperature, any acceleration gap must have finite spatial extent, and other realities must be considered. Ultimately, laboratory constraints and other physics limitations placed finite upper bounds on the achievable compression factors and minimum pulse lengths.

This paper employed PIC simulations in order to evaluate the neutralized drift compression of intense ion beams, and systematically studied the inclusion of various realistic effects in order to assess the upper limits of

longitudinal compression in the laboratory compared to the ideal (Sec. III). Quantitative examples examined the dependence of longitudinal compression on many system parameters, such as the finite-size acceleration gap and voltage waveform (Sec. III.A), initial beam temperature  $T_b$  (Sec. III.B), initial pulse length  $t_p$  and intended fractional tilt  $f$  (Sec. III.C), and variations in initial beam kinetic energy  $E_0$  and distribution (Sec. III.D).

First, ideal and realistic types of acceleration gap and voltage waveform (the infinitely thin and 3 cm long gaps and “sharp” and “smooth” waveforms, respectively) were studied in order to ascertain the origin of various effects. The electric field encountered by the beam in the gap had significant extent in space and time, relative to the initial bunch length  $L_b$  and  $t_p$  of the beam, and gave rise to a number of complications. For example, the finite-size gap was shown to impart an effective longitudinal temperature to an otherwise cold beam due to the coupling of transverse and longitudinal dynamics. Also, the inclusion of the extra voltage in the “smooth” compared to the “sharp” waveform increased the relative  $f$  and compression ratio by approximately 1/3 with only a small increase in minimum pulse duration at focus.

Second, it was shown that beam temperature, whether present in the initial beam or imparted by the gap, contributed to aberration of the focal plane, resulting in decreased amounts of compression, increased pulse lengths, and increased axial tolerance for diagnostic or target positioning. An analytical equation was derived for the minimum pulse length of an ideally-tilted beam with finite  $T_b$ , and accounted for the variation in aberration. The calculation agreed well with PIC simulation, when a constant accounted for the effective 45%  $T_b$  increase due to the “smooth” waveform and finite-size gap effects, for the parameters under consideration. The compression ratio and pulse length at focus were demonstrated to decrease and increase, respectively, with  $\sqrt{T_b}$  dependence, which was the limiting physics on longitudinal compression using optimized waveforms and plentiful plasma supply. Beam temperatures consistent with measurements reduced the achievable compression ratios to  $< 500$  for NDCX-relevant parameters, and caused asymmetric current profiles away from the focal plane. Theory and simulation revealed that slower head particles suffer from aberration more than faster tail particles.

Third, the axial compression dependence on initial  $t_p$  and intended  $f$  was also investigated, since they comprised the two voltage waveform  $V(t)$  parameters adjustable by the experimenter. The finite-size gap reduced the intended fractional tilt  $f$  as a function of the initial  $L_b$  and  $t_p$  compared to the gap size and transit time, and should also be considered an effective longitudinal temperature increase. Shorter initial  $t_p$  achieved reduced tilts from the gap effects, as the particle transit times became a significant fraction of  $t_p$ . A plateau effect in initial  $t_p$  was shown to occur, where aberrations due to longer drift lengths dominated increases in compression, indicating a trade-off consideration between current compres-

sion and pulse duration. The dependence on intended  $f$  was discussed and agreed well with theory. Larger tilts are generally desirable in experiments, but their realization is limited by the Volt-second capability and hold-off requirements of the induction module, as well as concerns over increased transverse focusing aberration. A balance between longer initial  $t_p$  and larger  $f$  was discussed, since both increased the compression ratio, but had opposite effects on the minimum pulse length  $t_{fwhm}$ , drift length  $L_d$ , and aberration. An optimum  $L_d$  was argued to exist, for a given set of beam parameters, that balances the competing effects determining the compression ratios and minimum pulse lengths at focus.

Fourth, quantitative examples presented in this paper outlined the dependence of axial compression on initial kinetic energy, whether constant in time or not, and distribution variations. Since the slope of the waveform was only ideal for one particular  $E_0$  and assumed a cold beam, simulations warned that small constant differences and temporal drifts in  $E_0$ , whether due to shot-to-shot variation, systematic uncertainty or inaccuracy, or hardware limitations, caused significant departure from the optimum compression parameters. It was also demonstrated that experimental beam energy scans to align the plane of the diagnostic with a peak compression result, while holding the waveform fixed, did not unambiguously determine the optimum compression, and a method for doing so was provided. Lastly, the beam's thermal distribution also affected the temporal shape of the current profiles and amount of aberration at focus. Beams with Waterbag distributions were shown to result in markedly asymmetric current profiles and reduced compression ratios, compared to the bell-shaped Maxwellian distribution results.

Future experiments seek to transversely focus a beam to a sub-mm spot coincident with the longitudinal focal plane using a strong final-focus solenoid (Sec. IV), in order to offset the radial defocusing effect inherent in the procedure of applying an axial velocity tilt (Sec. IV.A). However, transverse and longitudinal focusing aberrations occurred due to the variations in beam radius and axial beam energies entering the solenoid (Sec. IV.B).

Simulations involving beams with various initial  $r_b(t)$  and  $J_z(t)$  showed the simultaneous compression dependence on the beam's phase space, due to the coupling of the transverse and longitudinal dynamics within the solenoid. The transverse defocusing effect pulse-shaped a uniform beam into one with a triangular (or, parabolic)  $r_b(t)$  profile and was shown to be beneficial for compression, compared to the constant  $r_b(t)$  case, for reducing simultaneous focusing aberration within the constant solenoidal  $\mathbf{B}(r, z)$  fields.

In summary, no universally valid analytic model exists for determining the expected current compression ratio (and minimum pulse length) at focus because of the general intractability of including its dependence on many parameters, such as voltage waveform accuracy and finite-size acceleration gap geometry, beam parameters including the temperature and distribution type, neutralization processes by the background plasma, and other deleterious effects. Therefore, PIC simulations were employed as the most self-consistent method for investigating many of the major realistic effects that contribute to the physical and technological limits of longitudinal compression in the laboratory.

Future publications in this area will evaluate experimental plasma source flow profiles as well as address the cumulative effects of partial neutralization on charge bunch compression, such as increases to the beam's minimum radius, emittance, and minimum pulse length (to a lesser extent) at the simultaneous focal plane.

## VI. ACKNOWLEDGMENTS

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