

# Nonlinear $\delta f$ simulation studies of intense charged particle beams with large temperature anisotropy

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(Received 28 January 2002; accepted 12 April 2002)

In this paper, a 3D nonlinear perturbative particle simulation code (BEST) [H. Qin, R. C. Davidson, and W. W. Lee, *Phys. Rev. ST Accel. Beams* **3**, 084401 (2000)] is used to systematically study the stability properties of intense non-neutral charged particle beams with large temperature anisotropy ( $T_{\perp b} \gg T_{\parallel b}$ ). The most unstable modes are identified, and their eigenfrequencies, radial mode structure, and nonlinear dynamics are determined for axisymmetric perturbations with  $\partial/\partial\theta=0$ . © 2002 American Institute of Physics. [DOI: 10.1063/1.1484390]

## I. INTRODUCTION

Periodic focusing accelerators, transport systems, and storage rings<sup>1–5</sup> have a wide range of applications ranging from basic scientific research in high energy and nuclear physics, to applications such as heavy ion fusion, spallation neutron sources, tritium production, and nuclear waste transmutation, to mention a few examples. Of particular importance at the high beam currents and charge densities of practical interest, are the effects of the intense self-fields produced by the beam space charge and current on determining the detailed equilibrium, stability, and transport properties. While considerable progress has been made in understanding the self-consistent evolution of the beam distribution function,  $f_b(\mathbf{x}, \mathbf{p}, t)$ , and self-generated electric and magnetic fields,  $\mathbf{E}^s(\mathbf{x}, t)$  and  $\mathbf{B}^s(\mathbf{x}, t)$ , in kinetic analyses based on the nonlinear Vlasov–Maxwell equations,<sup>1,6–10</sup> in numerical simulation studies of intense beam propagation,<sup>11–19</sup> and in macroscopic warm-fluid models,<sup>20–23</sup> the effects of finite geometry and space-charge effects often make predictions of detailed stability behavior difficult. It is therefore important to develop an improved understanding of fundamental collective stability properties, including the case where a large temperature anisotropy ( $T_{\perp b} \gg T_{\parallel b}$ ) can drive a Harris-type instability,<sup>24,25</sup> familiar in the study of electrically neutral plasmas.

It is well known that in neutral plasmas with strongly anisotropic distributions ( $T_{\parallel b}/T_{\perp b} \ll 1$ ) a collective instability may develop if there is sufficient coupling between the transverse and longitudinal degrees of freedom.<sup>24,25</sup> Such anisotropies develop naturally in accelerators, where the longitudinal temperature of the accelerated beam of charged particles with charge  $q$  accelerated by a voltage  $V$  is reduced according to  $T_{\parallel bf} = T_{\parallel bi}^2/2qV$  (for a nonrelativistic beam). At the same time, the transverse temperature may increase due to nonlinearities in the applied and self-field forces, nonstationary beam profiles, and beam mismatch. These processes provide the free energy to drive collective instabilities and may lead to a deterioration of beam quality.<sup>18,26,27</sup> Historically, this instability was first studied analytically by Wang and Smith<sup>8</sup> for beams with a Kapchinkij–Vladimirskij (KV) distribution. Friedman *et al.*<sup>28–30</sup> reported a rapid “equilibra-

tion” process observed in 3D particle simulations of KV beams with large temperature anisotropy using the WARP code. They conjectured that the initial rapid heating in the longitudinal direction may be the result of an anisotropy-driven instability reminiscent of a Harris mode, but with transverse betatron motion instead of cyclotron motion. Realizing the fact that the highly inverted KV distribution may introduce numerous unstable modes, Lund *et al.*<sup>31,32</sup> used a semi-Gaussian distribution to carry out particle-in-cell simulations of the instability. However, unlike the KV distribution, the semi-Gaussian distribution is not a rigorous equilibrium solution of the Vlasov–Maxwell equations. The departure from a self-consistent equilibrium inevitably leads to mode excitations which can be confused with those due to the anisotropy-driven instability. The bi-Maxwellian distribution considered in the present study is a rigorous steady-state equilibrium of the Vlasov–Maxwell equations, and it does not support the spurious modes of the KV distribution. In addition, the bi-Maxwellian distribution is known to be a stable equilibrium with respect to transverse perturbations,<sup>9</sup> and therefore is an ideal candidate for studying instabilities driven by temperature anisotropy. A simple theory of the instability for a bi-Maxwellian distribution is presented in this paper, which appears to capture its main features and is a relatively straightforward generalization of the analysis of the Harris instability to the case of an intense particle beam. In this paper, we present the instability thresholds obtained in the simulations, as well as detailed simulations of the nonlinear development and saturation of the instability. We identify the main saturation mechanism as quasilinear stabilization due to resonant wave–particle interaction (Landau damping). A 3D nonlinear perturbative particle simulation code,<sup>14–16</sup> called the Beam Equilibrium, Stability, and Transport (BEST) code, is used to systematically study the electrostatic stability properties of intense nonneutral charged particle beams with large temperature anisotropy ( $T_{\perp b} \gg T_{\parallel b}$ ). The most unstable modes are identified, and their eigenfrequencies, radial mode structure, and nonlinear dynamics are determined for axisymmetric perturbations with  $\partial/\partial\theta=0$ . Since a well-behaved bi-Maxwellian distribution is used in the simulations, the mode structures observed are

different from those of the KV distribution previously reported.

The organization of this paper is the following: In Sec. II, we present a simple kinetic model of the instability based on a matrix dispersion equation derived from the linearized Vlasov–Poisson equations. The nonlinear  $\delta f$  simulation method is briefly described in Sec. III, and in Sec. IV we present detailed simulation results for a wide range of system parameters.

## II. LINEAR STABILITY THEORY

### A. Kinetic description

Wang and Smith<sup>8</sup> investigated the kinetic stability properties of an intense particle beam assuming a Kapchinkij–Vladimirskij (KV) beam distribution<sup>6</sup> in the limit of large energy anisotropy ( $T_{\parallel b}/T_{\perp b} \rightarrow 0$ ) by expanding the solution of the linearized Vlasov–Poisson equations in a series of Gluckstern eigenfunctions  $\delta\varphi_n(r) = (1/2)[P_{n-1}(1 - 2r^2/r_b^2) + P_n(1 - 2r^2/r_b^2)]$ , where  $P_n(x)$  is the  $n$ th-order Legendre polynomial.<sup>7</sup> The expansion yields a dispersion relation, expressible in terms of an infinite matrix determinant. For long-wavelength axial perturbations with  $k_z^2 r_b^2 \ll 1$ , one-half of the modes<sup>8</sup> are identified as transverse ( $T_n$ ) Gluckstern modes with eigenfunction  $\delta\varphi \propto \delta\varphi_n$ . The other half<sup>8</sup> consists of modes corresponding in the limit of large tune depression ( $\nu \rightarrow 0$ ) to an ordinary cold-beam longitudinal mode ( $L_1$ ) with eigenfunction  $\delta\varphi \propto J_0(k_z r)$  inside the beam and dispersion relation  $(\omega - k_z V_b)^2 = (\hat{\omega}_{pb}^2/2)(k_z r_b)^2 \ln(r_w/r_b)$ , plus a less-known class of “coupling” modes ( $L_n$ ) with  $\delta\varphi \propto \delta\varphi_n$  and  $(\omega - k_z V_b)^2 = [\hat{\omega}_{pb}^2/8n(n+1)](k_z r_b)^2 \int_0^\pi (dx/2\pi) \times P_n(\cos x)$ . The latter modes are the result of the interaction between transversely oscillating particles and the longitudinal perturbed potential. Here,  $\omega$  is the mode oscillation frequency,  $k_z$  is the axial wavenumber of the perturbation,  $V_b = \beta c$  is the axial beam velocity, and  $J_0(x)$  is the ordinary Bessel function of the first kind of the order zero. Furthermore,  $\nu = \nu_0(1 - s_b)^{1/2}$  is the depressed tune, where  $s_b = \hat{\omega}_{pb}^2/2\gamma_b^2\omega_f^2$  is the normalized beam intensity,  $\hat{\omega}_{pb}^2 = 4\pi\hat{n}_b e_b^2/\gamma_b m_b$  is the relativistic plasma frequency-squared,  $\nu_0 = \omega_f$  is the transverse betatron frequency associated with the applied focusing field,  $r_b$  is the beam edge radius,  $r_w$  is the radius of the perfectly conducting wall,  $\gamma_b = (1 - \beta_b^2)^{-1/2}$  is the relativistic mass factor,  $e_b$  and  $m_b$  are the particle charge and rest mass, respectively, and  $\hat{n}_b$  is the number density of the beam particles.

As a general rule, for a KV distribution, instability arises in the regions of parameter space where two or more modes interact resonantly. The transverse modes ( $T_n$ ) are not significantly affected by longitudinal perturbations, and therefore the instability due to their interaction is a consequence of the fact that the KV distribution has a highly inverted population in phase space.<sup>1,6–8</sup> The most dangerous  $T_n$ – $L_k$  instabilities are due to  $T_2$ – $L_1$  interactions<sup>8</sup> in the region where  $\nu/\nu_0 \approx 0.44$  with maximum growth rate  $\text{Im } \omega/\nu_0 \approx 0.03$ , and due to  $T_2$ – $L_2$  interactions in the region  $0.2 \leq \nu/\nu_0 \leq 0.32$ , with maximum growth rate  $\text{Im } \omega/\nu_0 \approx 0.15$ . The latter mode has a much higher growth rate due to the

similar transverse structure of the  $L_2$  and  $T_2$  modes. The growth rate obtained by Wang and Smith<sup>8</sup> is a maximum for  $k_z^2 r_b^2 \approx 1$  in both cases.

It is important to extend theoretical studies of the kinetic stability properties of anisotropic beams to distribution functions other than the KV distribution. This is because the KV distribution has an (unphysical) inverted population in transverse phase-space variables, which provides the free energy to drive collective instabilities at high beam intensities that are intrinsic to this inverted population.<sup>7,8</sup> This, of course, can mask the effects of anisotropy-driven instabilities. To this end, we briefly outline here a simple derivation of the Harris-type instability<sup>24,25</sup> in intense particle beams for electrostatic perturbations about the thermal equilibrium distribution with temperature anisotropy ( $T_{\perp b} > T_{\parallel b}$ ) described in the beam frame by the self-consistent axisymmetric Vlasov equilibrium,<sup>1,10</sup>

$$f_b^0(r, \mathbf{p}) = \frac{\hat{n}_b}{(2\pi m_b T_{\perp b})} \exp\left(-\frac{H_{\perp}}{T_{\perp b}}\right) \frac{1}{(2\pi m_b T_{\parallel b})^{1/2}} \times \exp\left(-\frac{p_z^2}{2m_b T_{\parallel b}}\right). \quad (1)$$

Here,  $H_{\perp} = p_{\perp}^2/2m_b + (1/2)m_b\omega_f^2(x^2 + y^2) + e_b\phi^0(r)$  is the single-particle Hamiltonian,  $p_{\perp} = (p_x^2 + p_y^2)^{1/2}$  is the transverse particle momentum,  $r = (x^2 + y^2)^{1/2}$  is the radial distance from the beam axis,  $\omega_f = \text{const.}$  is the transverse frequency associated with the applied focusing field, and  $\phi^0(r)$  is the equilibrium space-charge potential determined self-consistently from Poisson’s equation,  $r^{-1}(\partial/\partial r)(r\partial\phi^0/\partial r) = -4\pi e_b n_b^0$ , where  $n_b^0(r) = \int d^3p f_b^0(r, \mathbf{p})$  is the equilibrium number density of beam particles. For simplicity, the analysis is carried out in the beam frame ( $V_b = 0$  and  $\gamma_b = 1$ ). Furthermore, setting  $\phi^0(r=0) = 0$ , the constant  $\hat{n}_b$  occurring in Eq. (1) can be identified with the on-axis density  $n_b^0(r=0)$ , and the constants  $T_{\perp b}$  and  $T_{\parallel b}$  can be identified with the transverse and longitudinal temperatures (energy units), respectively.

For present purposes, we consider small-amplitude, axisymmetric ( $\partial/\partial\theta = 0$ ) electrostatic perturbations of the form,

$$\delta\phi(\mathbf{x}, t) = \widehat{\delta\phi}(r) \exp(ik_z z - i\omega t), \quad (2)$$

where  $\delta\phi(\mathbf{x}, t)$  is the perturbed electrostatic potential,  $k_z$  is the axial wave number, and  $\omega$  is the complex oscillation frequency, with  $\text{Im } \omega > 0$  corresponding to instability (temporal growth). Without presenting algebraic details, using the method of characteristics, the linearized Poisson equation can be expressed as

$$\frac{1}{r} \frac{\partial}{\partial r} r \frac{\partial}{\partial r} \widehat{\delta\phi}(r) - k_z^2 \widehat{\delta\phi}(r) = -4\pi e_b \int d^3p \widehat{\delta f_b}(r, \mathbf{p}), \quad (3)$$

where

$$\widehat{\delta f}_b(r, \mathbf{p}) = -\frac{e_b}{T_{\perp b}} \widehat{\delta \phi} f_b^0 - \frac{e_b}{T_{\perp b}} \left[ \omega - k_z v_z \left( 1 - \frac{T_{\perp b}}{T_{\parallel b}} \right) \right] f_b^0 \times i \int_{-\infty}^t dt' \widehat{\delta \phi}[r'(t')] \exp[i(k_z v_z - \omega)(t' - t)] \quad (4)$$

for perturbations about the choice of the anisotropic thermal equilibrium distribution function in Eq. (1). In the orbit integral in Eq. (4),  $\text{Im } \omega > 0$  is assumed, and  $r'(t') = [x'^2(t') + y'^2(t')]^{1/2}$  is the radial orbit in the equilibrium field configuration such that  $[\mathbf{x}'_>(t'), \mathbf{p}'_>(t')]$  passes through the phase-space point  $(\mathbf{x}_>, \mathbf{p}_>)$  at time  $t' = t$ . We express the perturbation amplitude as  $\widehat{\delta \phi}(r) = \sum_n \alpha_n \phi_n(r)$ , where  $\{\alpha_n\}$  are constants, and the complete set of vacuum eigenfunctions  $\{\phi_n(r)\}$  is defined by  $\phi_n(r) = A_n J_0(\lambda_n r/r_w)$ . Here,  $\lambda_n$  is the  $n$ th zero of  $J_0(\lambda_n) = 0$ , and  $A_n = \sqrt{2}/[r_w J_1(\lambda_n)]$  is a normalization constant such that  $\int_0^{r_w} dr r \phi_n(r) \phi_{n'}(r) = \delta_{n,n'}$ . We substitute  $\widehat{\delta \phi}(r) = \sum_n \alpha_n \phi_n(r)$  into Poisson's equation (3) and operate with  $\int_0^{r_w} dr r \phi_n(r) \dots$ . This gives the matrix dispersion equation

$$\sum_n \alpha_n D_{n,n'}(\omega) = 0, \quad (5)$$

where

$$D_{n,n'}(\omega) = (\lambda_n^2 + k_z^2 r_w^2) \delta_{n,n'} + \chi_{n,n'}(\omega), \quad (6)$$

and the beam-induced susceptibility  $\chi_{n,n'}(\omega)$  is defined by

$$\chi_{n,n'}(\omega) = -4 \pi e_b r_w^2 \int_0^{r_w} dr r \phi_{n'}(r) \int d^3 p \widehat{\delta f}_b^n(r, \mathbf{p}). \quad (7)$$

Here,  $\widehat{\delta f}_b^n(r, \mathbf{p})$  is defined in Eq. (4) with  $\widehat{\delta \phi} \rightarrow \phi_n$ . The condition for a nontrivial solution to Eq. (5) is

$$\det\{D_{n,n'}(\omega)\} = 0, \quad (8)$$

which plays the role of a matrix dispersion relation that determines the complex oscillation frequency  $\omega$ .

We defer a detailed analysis of Eqs. (5)–(8) to a separate paper, and summarize here some *qualitative* properties of the Harris-type instability that ensues in the limit of an anisotropic beam distribution that is *cold* in the longitudinal direction, i.e.,

$$\frac{T_{\parallel b}}{T_{\perp b}} \rightarrow 0. \quad (9)$$

In this regard, it is convenient to introduce the effective *depressed* betatron frequency  $\omega_{\beta\perp}$ . It can be shown<sup>1</sup> that for the equilibrium distribution in Eq. (1), the mean-square beam radius  $r_b^2$  defined by

$$r_b^2 = \langle r^2 \rangle = \frac{\int dr r^3 n_b^0(r)}{\int dr r n_b^0(r)}, \quad (10)$$

is related exactly to the line density  $N_b = 2\pi \int dr r n_b^0(r)$ , and transverse beam temperature  $T_{\perp b}$  by the equilibrium radial force balance equation,<sup>1</sup>

$$\omega_f^2 r_b^2 = \frac{N_b e_b^2}{m_b} + \frac{2T_{\perp b}}{m_b}. \quad (11)$$

Equation (11) can be rewritten as

$$\left( \omega_f^2 - \frac{1}{2} \bar{\omega}_{pb}^2 \right) r_b^2 = \frac{2T_{\perp b}}{m_b}, \quad (12)$$

where we have introduced the effective *average* beam plasma frequency  $\bar{\omega}_{pb}$  defined by

$$r_b^2 \bar{\omega}_{pb}^2 \equiv \int_0^{r_w} dr r \omega_{pb}^2(r) = \frac{2e_b^2 N_b}{m_b}. \quad (13)$$

Then, Eq. (12) can be used to introduce the effective *depressed* betatron frequency  $\omega_{\beta\perp}$  defined by

$$\omega_{\beta\perp}^2 \equiv \left( \omega_f^2 - \frac{1}{2} \bar{\omega}_{pb}^2 \right) = \frac{2T_{\perp b}}{m_b r_b^2}. \quad (14)$$

If, for example, the beam density were uniform over the beam cross section, then Eq. (14) corresponds to the usual definition of the depressed betatron frequency for a KV beam, and it's readily shown that the radial orbit  $r'(t')$  occurring in Eqs. (4) and (7) can be expressed as<sup>1</sup>

$$r'^2(t') = r^2 \cos^2(\omega_{\beta\perp} \tau) + \frac{p_{\perp}^2}{m_b^2 \omega_{\beta\perp}^2} \sin^2(\omega_{\beta\perp} \tau) + \frac{r p_{\perp}}{m_b \omega_{\beta\perp}} \cos(\phi - \theta) \sin(2\omega_{\beta\perp} \tau). \quad (15)$$

Here  $\tau = t' - t$  is the displaced time variable, and we have expressed  $(x, y) = (r \cos \theta, r \sin \theta)$  and  $(p_x, p_y) = (p_{\perp} \cos \phi, p_{\perp} \sin \phi)$  in cylindrical polar coordinates. Note from Eq. (15) that  $r'(t' = t) = r$  and  $[dr'^2/dt']_{t'=t} = 2(x p_x + y p_y)/m_b$ , as expected. Due to the nontrivial dependence of the perturbed potential in Eq. (4) on radius  $r$ , the transverse betatron motion [Eq. (15)] will drive density perturbations resonantly at frequencies that are multiples of  $2\omega_{\beta\perp}$ . Instability occurs when one of these frequencies is close to the beam plasma frequency  $\omega_{pb}$ .

In general, for the choice of equilibrium distribution function in Eq. (1), there will be a spread in transverse depressed betatron frequencies  $\omega_{\beta\perp}(H_{\perp})$ , and the particle trajectories will not be described by the simple trigonometric function in Eq. (15). For present purposes, however, we consider a simple *model* in which the radial orbit  $r'(t')$  occurring in Eq. (4) and the definition of  $\chi_{n,n'}(\omega)$  in Eq. (7) is approximated by Eq. (15) with the constant value  $\omega_{\beta\perp}$  defined in Eq. (14) and the *approximate* equilibrium density profile defined by  $n_b^0(r) = \hat{n}_b \exp(-m_b \omega_{\beta\perp}^2 r^2 / 2T_{\perp b})$ . For a nonuniform beam,  $\omega_{\beta\perp}^{-1}$  is the characteristic time for a particle with thermal speed  $v_{\text{th}\perp} = (2T_{\perp b}/m_b)^{1/2}$  to cross the rms radius  $r_b$  of the beam. In this case,  $\chi_{n,n'}(\omega)$  can be evaluated in closed analytical form provided the conducting wall is sufficiently far removed from the beam ( $r_w/r_b \gg 3$ , say). In this case, the matrix elements decrease exponentially away from the diagonal, with

$$\left| \frac{D_{n,n+k}}{D_{n,n}} \right| \sim \exp\left(-\frac{\pi^2 k^2}{4} \frac{r_b^2}{r_w^2}\right), \quad (16)$$

where  $k$  is an integer, and we have used the approximate relation  $\lambda_n \approx \pi(4n-1)/4$ . Therefore, for  $r_w/r_b \gtrsim 3$ , we can approximate  $\{D_{n,n'}(\omega)\}$  by a *tridiagonal* matrix. In this case, for the lowest-order radial modes ( $n=1$  and  $n=2$ ), the matrix dispersion relation (8) can be approximated by

$$\begin{aligned} & \left\{ \lambda_1^2 + k_z^2 r_w^2 + \frac{2 \exp(-k_1^2/2)(\hat{\omega}_p^2/\omega_{\beta\perp}^2)}{J_1^2(\lambda_1)} \left[ I_0\left(\frac{k_1^2}{2}\right) - \left(1 + \frac{k_z^2 v_{\text{th}\perp}^2}{2\omega^2}\right) I_0^2\left(\frac{k_1^2}{4}\right) - \left(\frac{\omega}{\omega - 2\omega_{\beta\perp}} + \frac{k_z^2 v_{\text{th}\perp}^2}{2(\omega - 2\omega_{\beta\perp})^2}\right) I_1^2\left(\frac{k_1^2}{4}\right) \right] \right\} \\ & \times \left\{ \lambda_2^2 + k_z^2 r_w^2 + \frac{2 \exp(-k_2^2/2)(\hat{\omega}_p^2/\omega_{\beta\perp}^2)}{J_1^2(\lambda_2)} \left[ I_0\left(\frac{k_2^2}{2}\right) - \left(1 + \frac{k_z^2 v_{\text{th}\perp}^2}{2\omega^2}\right) I_0^2\left(\frac{k_2^2}{4}\right) - \left(\frac{\omega}{\omega - 2\omega_{\beta\perp}} + \frac{k_z^2 v_{\text{th}\perp}^2}{2(\omega - 2\omega_{\beta\perp})^2}\right) I_1^2\left(\frac{k_2^2}{4}\right) \right] \right\} \\ & = \frac{(2\hat{\omega}_p^2/\omega_{\beta\perp}^2)^2}{J_1^2(\lambda_1)J_1^2(\lambda_2)} \exp\left(-\frac{(k_1^2+k_2^2)}{2}\right) \left\{ I_0\left(\frac{k_1 k_2}{2}\right) - \left(1 + \frac{k_z^2 v_{\text{th}\perp}^2}{2\omega^2}\right) I_0^2\left(\frac{k_1 k_2}{4}\right) - \left(\frac{\omega}{\omega - 2\omega_{\beta\perp}} + \frac{k_z^2 v_{\text{th}\perp}^2}{2(\omega - 2\omega_{\beta\perp})^2}\right) I_1^2\left(\frac{k_1 k_2}{4}\right) \right\}^2, \quad (18) \end{aligned}$$

where we have retained only the leading-order nonresonant terms and one resonant term at (positive) frequency  $\omega \approx 2\omega_{\beta\perp}$ . In the dispersion relation (18),  $\lambda_1 \approx 2.405$  and  $\lambda_2 \approx 5.52$  are determined from the zeros of  $J_0(\lambda_n)=0$ ,  $v_{\text{th}\perp} = (2T_{\perp b}/m_b)^{1/2}$  is the transverse thermal speed,  $k_1$  and  $k_2$  are defined by  $k_1 = \lambda_1 r_b/r_w$  and  $k_2 = \lambda_2 r_b/r_w$ , and  $\omega_{\beta\perp} = \omega_f(1-\bar{s}_b)^{1/2}$  is the effective depressed betatron frequency [Eq. (14)], where  $\bar{s}_b = \hat{\omega}_{pb}^2/2\omega_f^2$  is the effective normalized beam intensity defined in terms of  $\hat{\omega}_{pb}$ .

The dispersion relation (18) can be used to investigate detailed electrostatic stability properties for strong anisotropy ( $T_{\parallel b}/T_{\perp b} \rightarrow 0$ ) for a wide range of normalized axial wave numbers ( $k_z r_w$ ) and effective normalized beam intensity  $\bar{s}_b = \hat{\omega}_{pb}^2/2\omega_f^2$ , or equivalently, normalized tune depression  $\bar{\nu}/\nu_0$  defined by

$$\frac{\bar{\nu}}{\nu_0} \equiv \frac{\omega_{\beta\perp}}{\omega_f} = (1-\bar{s}_b)^{1/2}. \quad (19)$$

For sufficiently large  $k_z r_w$ , the large temperature anisotropy ( $T_{\parallel b}/T_{\perp b} \rightarrow 0$ ) in Eq. (18) provides the free energy to drive the classical Harris-type instability,<sup>24,25</sup> generalized here to include finite transverse geometry and beam space-charge effects. The influence of the finite longitudinal temperature can be taken into account if one assumes  $T_{\parallel b} \neq 0$  in Eq. (1). This results in the (collisionless) Landau damping of the unstable mode due to resonant wave-particle interactions<sup>1</sup> associated with the axial momentum spread of the beam particles.

To compare with the simulation results in Sec. IV, we introduce the normalized beam intensity  $s_b$  defined in terms of the on-axis ( $r=0$ ) beam density  $\hat{n}_b$ . Here,  $s_b \equiv \hat{\omega}_{pb}^2/2\omega_f^2$ , where  $\hat{\omega}_{pb} = (4\pi e_b^2 \hat{n}_b/m_b)^{1/2}$ . Using Eqs. (11)–(14), the normalized beam intensity  $\bar{s}_b = \hat{\omega}_{pb}^2/2\omega_f^2$  introduced in Eq. (19) is related to  $s_b$  by the equation

$$D_{1,1}(\omega)D_{2,2}(\omega) - [D_{1,2}(\omega)]^2 = 0, \quad (17)$$

where use has been made of  $D_{1,2}(\omega) = D_{2,1}(\omega)$ .

We introduce the effective perpendicular thermal speed squared of a beam particle defined by  $v_{\text{th}\perp}^2 = 2T_{\perp b}/m_b$ . Then, for  $T_{\parallel b}/T_{\perp b} \rightarrow 0$  and  $r_w/r_b \gtrsim 3$ , the approximate dispersion relation (17) describing the coupling of the lowest order  $n=1$  mode with the  $n=2$  radial mode, within the context of the present simplified model, can be expressed as

$$s_b = \bar{s}_b \hat{n}_b \left( \int_0^{r_w} dr r^3 n_b^0(r) \right) / \left( \int_0^{r_w} dr r n_b^0(r) \right)^2. \quad (20)$$

The allowed range of the normalized intensity parameter  $s_b$  is  $0 \leq s_b < 1$ , where the limit  $s_b \rightarrow 1$  corresponds to infinitely depressed tune (space-charge-dominated limit).

Typical numerical results obtained from the approximate dispersion relation (18) are presented in Figs. 1–5 for the case where  $r_w = 3r_b$ . Figure 1 shows the normalized growth rate  $(\text{Im } \omega)/\omega_f$  plotted vs normalized wave number  $k_z r_w$  for several values of normalized on-axis beam intensity  $s_b$ . Note from Fig. 1 that the critical value of  $k_z r_w$  for the onset of instability increases as  $s_b$  is decreased, and that the maximum normalized growth rate  $(\text{Im } \omega)_{\text{max}}/\omega_f$  is achieved for  $s_b = 0.96$  (Fig. 2). In the limit where  $k_z r_w \rightarrow \infty$ , the growth rate is zero for  $s_b < 0.75$ . Finite  $T_{\parallel b}$  effects introduce a finite bandwidth in  $k_z r_w$  for instability, since the modes with large values of  $k_z r_w$  are stabilized by Landau damping. Therefore, the stability results in Figs. 2 and 4,5 are plotted for moderate value of normalized wave number corresponding to  $k_z r_w = 8$ .

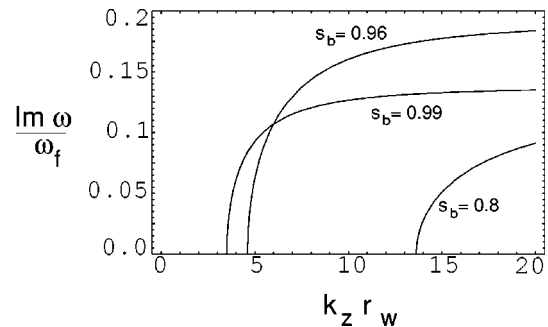


FIG. 1. Plot of  $(\text{Im } \omega)/\omega_f$  vs  $k_z r_w$  obtained from Eq. (18) for  $r_w = 3r_b$  and several values of normalized beam intensity  $s_b$ , defined in Eq. (20).



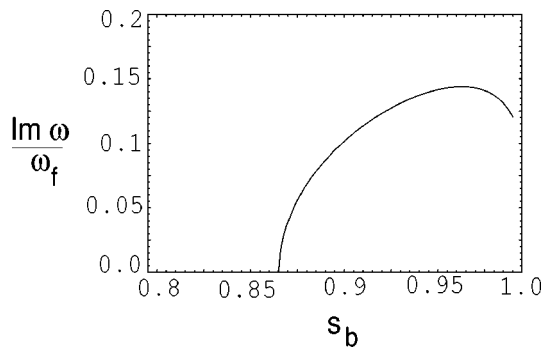


FIG. 2. Plot of  $(\text{Im } \omega)/\omega_f$  vs normalized beam intensity  $s_b$  obtained from Eq. (18) for  $r_w=3r_b$  and  $k_z r_w=8$ .

Figure 3 shows the normalized real oscillation frequency  $(\text{Re } \omega)/\omega_f$  plotted vs normalized wave number  $k_z r_w$  for  $s_b=0.96$ . The high-frequency branches correspond to transverse modes that are present when  $k_z r_w=0$ . The low-frequency branches correspond to longitudinal modes that are absent when  $k_z r_w=0$ . For  $k_z r_w$  greater than some threshold value, the intermediate high-frequency longitudinal mode and the low-frequency transverse mode coalesce and have the same value of real oscillation frequency,  $(\text{Re } \omega)/\omega_f \approx 0.8$ , with growth rate  $(\text{Im } \omega)/\omega_f$  given by the  $s_b=0.96$  curve in Fig. 1.

The corresponding behavior of the normalized real oscillation frequency  $(\text{Re } \omega)/\omega_f$  as a function of  $s_b$  for fixed  $k_z r_w=8$  is plotted in Fig. 4. For  $s_b$  greater than some threshold value, the two branches coalesce. The real oscillation frequency of the resulting branch is a weak function of  $s_b$ . The existence of instability thresholds, both for  $k_z r_w$  and  $s_b$ , is a reflection of the resonant nature of the instability. Indeed, referring to Eq. (18), the beam must be sufficiently intense for the beam plasma frequency to be close to the second harmonic of the effective depressed betatron frequency  $\omega_{\beta\perp}$  (Fig. 4). Also, since the longitudinal mode frequency is proportional to the normalized wave number  $k_z r_w$  (for  $k_z r_w \leq 5$ ) (Fig. 3), the resonant condition is achieved only for sufficiently large values of  $k_z r_w$ .

The normalized eigenfunction plots of  $\text{Re } \delta\hat{\phi}(r)$  and  $\text{Im } \delta\hat{\phi}(r)$  vs  $r/r_w$  corresponding to  $s_b=0.96$  and  $k_z r_w=8$  are plotted vs  $r/r_w$  in Fig. 5. The real part of the eigenfunc-

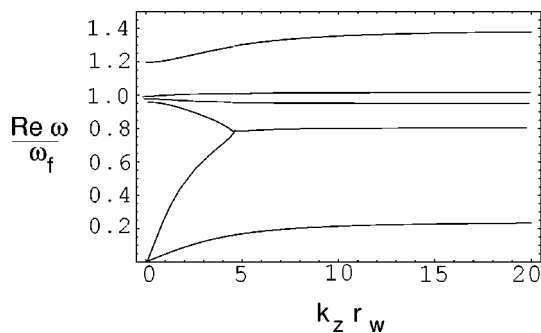


FIG. 3. Plot of  $(\text{Re } \omega)/\omega_f$  vs  $k_z r_w$  obtained from Eq. (18) for  $r_w=3r_b$  and  $s_b=0.96$ .

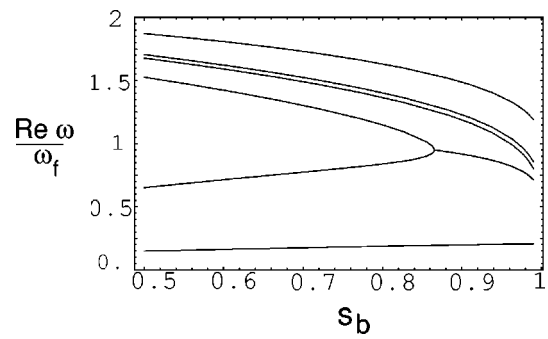


FIG. 4. Plot of  $(\text{Re } \omega)/\omega_f$  vs normalized beam intensity  $s_b$  obtained from Eq. (18) for  $r_w=3r_b$  and  $k_z r_w=8$ .

tion has no zeros, and has a structure similar to the familiar longitudinal mode ( $L_1$ ) in Ref. 8.

### B. Macroscopic warm-fluid description

To remedy the problem arising from an unphysical KV distribution, Strasburg and Davidson<sup>21,22</sup> employed a warm-fluid model<sup>20</sup> to investigate the stability properties of intense charged beams with large pressure anisotropy. A waterbag equilibrium and negligible heat-flow were assumed. For  $k_z=0$ , the model recovers stable high-frequency ( $\omega_n > \sqrt{2}\nu_0$ ) modes, which are similar to the stable high-frequency  $T_n$  modes of a KV beam, whereas the low-frequency unstable  $T_n$  modes are absent. For sufficiently large values of  $k_z^2 r_b^2$ , the anisotropy leads to instability provided the intensity of the beam is sufficiently below the space-charge limit,  $\nu/\nu_0 \geq 0.5$ . The maximum growth rate  $\text{Im } \omega/\nu_0 \approx 0.33$  is achieved for  $k_z^2 r_b^2 > 1$  and  $0.6 \leq \nu/\nu_0 \leq 0.9$ .

The assumption in the warm-fluid description is that the frequencies of the interest are much larger than the resonant frequencies characteristic of the transverse particle motion, so that the contribution from the resonant particles can be neglected. The same assumption allows one to neglect the heat-flow term in the equation for the pressure tensor. Hence, the low-frequency modes ( $\omega \approx \nu_0$ ) are not correctly described by such a warm-fluid model. In the warm-fluid treatment,<sup>21,22</sup> the instability arises as a resonant interaction of the smallest-frequency transverse fluid mode, and the ordinary longitudinal mode at frequency  $\omega \approx \nu_0$ . At this fre-

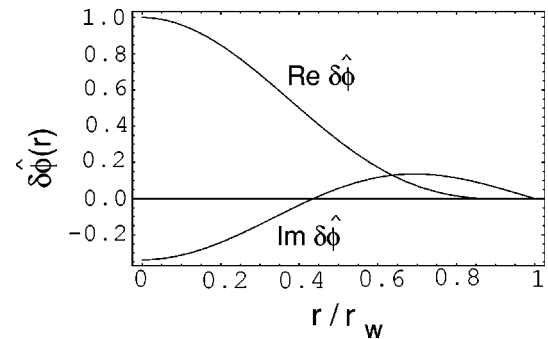


FIG. 5. Radial mode structure of the unstable eigenfunction for  $r_w=3r_b$ ,  $k_z r_w=8$ , and  $s_b=0.96$ .

quency one cannot neglect the resonant interaction with the transverse particle motion, and one must normally employ a kinetic description.

### III. DESCRIPTION OF THE NONLINEAR $\delta f$ SIMULATION CODE

The theoretical model described in Sec. II uses simplified assumptions for the background distribution function. In practical applications, the transverse distribution function may be close to thermal equilibrium with temperature  $T_{\perp b}$ , and the longitudinal distribution can be described by a drifting Maxwellian distribution with temperature  $T_{\parallel b} \ll T_{\perp b}$ . This distribution is stable with respect to transverse perturbations.<sup>1,9</sup> For an arbitrary equilibrium distribution one cannot solve the stability problem analytically and must employ numerical simulation techniques. To investigate stability properties numerically, we use the nonlinear  $\delta f$  method<sup>33</sup> described below, as implemented in the Beam Equilibrium, Stability, and Transport (BEST) code.<sup>14-16</sup>

In the smooth-focusing approximation, the transverse focusing force is modeled by  $\mathbf{F}_{\text{foc}} = -\gamma_b m_b \omega_f^2 \mathbf{x}_{\perp}$ , where  $\omega_f$  is the constant focusing frequency associated with applied focusing field,  $m_b$  is the particle rest mass,  $\gamma_b = (1 - \beta_b^2)^{-1/2}$  is the relativistic mass factor,  $\beta_b c = \text{const}$  is the average axial beam velocity, and  $c$  is the speed of light *in vacuo*. The solutions to the nonlinear Vlasov–Maxwell equations are expressed as  $f_b = f_b^0 + \delta f_b$ ,  $\phi = \phi^0 + \delta\phi$  and  $A_z = A_z^0 + \delta A_z$ , where  $(f_b^0, \phi^0, A_z^0)$  are known equilibrium solutions. The perturbed potentials satisfy the equations,<sup>14</sup>

$$\nabla^2 \delta\phi = -4\pi e_b \int d^3p \delta f_b, \quad (21)$$

$$\nabla^2 \delta A_z = -\frac{4\pi}{c} e_b \int d^3p v_z \delta f_b, \quad (22)$$

where  $e_b$  is the particle charge, and  $\delta f_b(\mathbf{x}, \mathbf{p}, t)$  is given by the weighted Klimontovich representation,

$$\delta f_b = \frac{N_b}{N_{sb}} \sum_{i=1}^{N_{sb}} w_{bi} \delta(\mathbf{x} - \mathbf{x}_{bi}) \delta(\mathbf{p} - \mathbf{p}_{bi}). \quad (23)$$

Here,  $N_{sb}$  is total number of beam simulation particles,  $N_b$  is total number of actual beam particles, and the weight function is defined by  $w_b \equiv \delta f_b / f_b$ .

The nonlinear particle simulations are carried out by iteratively advancing the particle motion, including the weights they carry, according to<sup>14</sup>

$$\frac{d\mathbf{x}_{bi}}{dt} = (\gamma_b m_b)^{-1} \mathbf{p}_{bi}, \quad (24)$$

$$\frac{d\mathbf{p}_{bi}}{dt} = -\gamma_b m_b \omega_f^2 \mathbf{x}_{\perp bi} - e_b \left( \nabla\phi - \frac{v_{zbi}}{c} \nabla_{\perp} A_z \right), \quad (25)$$

$$\frac{dw_{bi}}{dt} = -(1 - w_{bi}) \frac{1}{f_{b0}} \frac{\partial f_{b0}}{\partial \mathbf{p}} \cdot \delta \left( \frac{d\mathbf{p}_{bi}}{dt} \right), \quad (26)$$

$$\delta \left( \frac{d\mathbf{p}_{bi}}{dt} \right) = -e_b \left( \nabla\delta\phi - \frac{v_{zbi}}{c} \nabla_{\perp} \delta A_z \right), \quad (27)$$

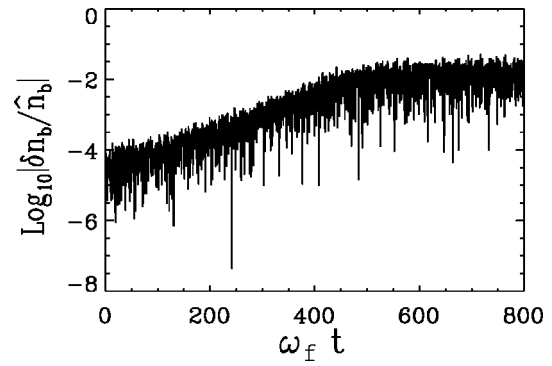


FIG. 6. Time history of the density perturbation  $\delta n_{\text{max}}/\hat{n}_b$  for normalized beam intensity  $s_b = 0.7$  at fixed  $z$  and  $r = 0.2r_b$ .

and updating the fields by solving the perturbed Maxwell's equations with appropriate boundary conditions at the cylindrical, perfectly conducting wall at radius  $r_w$ .

The  $\delta f$  approach is fully equivalent to the original nonlinear Vlasov–Maxwell equations, but the noise associated with representation of the background distribution  $f_b^0$  in conventional particle-in-cell (PIC) simulations is removed. In the  $\delta f$  approach, the simulation particles are used to represent only a small part of the entire distribution  $\delta f_b = f_b - f_b^0$ , and therefore the statistical error in the simulation is proportional to  $\epsilon_{\delta f} \sim \delta f_b / \sqrt{N_{sb}}$ , whereas the error in PIC simulations is proportional to  $\epsilon_{\text{pic}} \sim f_b / \sqrt{N_{sb}}$ . Therefore, the typical gain in accuracy in  $\delta f$  simulations compared to PIC simulations with the same number of particles is  $\epsilon_{\delta f} / \epsilon_{\text{pic}} = \bar{w}_{bi}$ .<sup>14</sup> This fact allows much more accurate simulations of the nonlinear dynamics and instability thresholds when  $|\bar{w}_{bi}| \ll 1$ . When the perturbation  $\delta f_b$  becomes comparable in magnitude with the background distribution function  $f_b^0$ , then the  $\delta f$  method becomes less accurate than a full PIC simulation. In the present paper, a hybrid combination of the  $\delta f$  and PIC simulation methods is used, where the number density is calculated according to  $\delta n_b = [1 - \theta(\bar{w}_{bi})] \delta n_{\delta f} + \theta(\bar{w}_{bi})(n_{\text{pic}} - n_0)$ , where  $\theta(w)$  is a monotonic function of its argument such that  $\theta(w \rightarrow 0) \rightarrow 0$  and  $\theta(w \rightarrow 1) \rightarrow 1$ . Here,  $\delta n_{\delta f} = \int d^3p \delta f_b$  and  $n_{\text{pic}} = \int d^3p f_b$ .

In addition, the  $\delta f$  method can be used to study linear stability properties, provided all nonlinear terms in the dy-

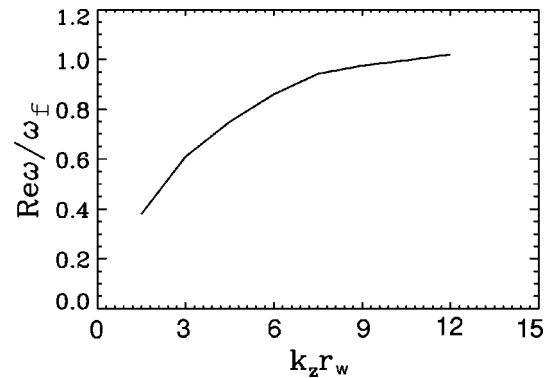


FIG. 7. Normalized eigenfrequency  $\text{Re}(\omega_f/\omega_f)$  plotted vs  $k_z r_w$  for  $s_b = 0.7$  and  $r_w = 3r_b$ , and initial  $T_{\parallel b}/T_{\perp b} = 0.04$ .

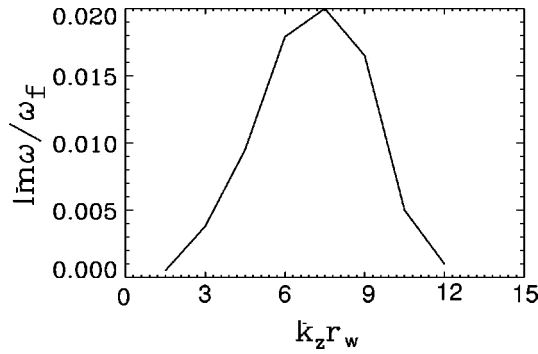


FIG. 8. Normalized growth rate  $\text{Im } \omega/\omega_f$  plotted vs  $k_z r_w$  for  $s_b=0.7$  and  $r_w=3r_b$ , and initial  $T_{\parallel b}/T_{\perp b}=0.04$ .

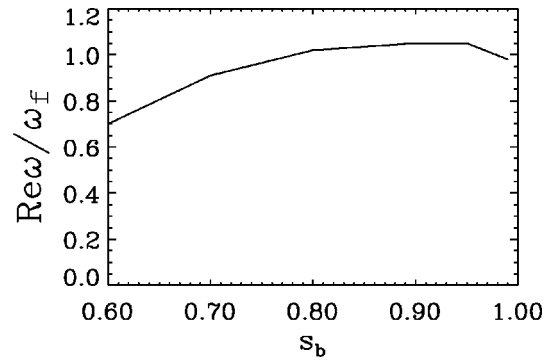


FIG. 10. Plot of  $(\text{Re } \omega)/\omega_f$  vs normalized beam intensity  $s_b$  for  $k_z r_w=7.5$  and  $r_w=3r_b$ , and initial  $T_{\parallel b}/T_{\perp b}=0.04$ .

namical equations (25)–(27) are neglected.<sup>14–16</sup> This corresponds to replacing the term  $1-w_{bi}$  with 1 in Eq. (26) for the weights, and moving particles along the trajectories calculated in the unperturbed potentials  $(\phi^0, A_z^0)$ .

The  $\delta f$  method described above has been implemented in the three-dimensional electromagnetostatic particle-in-cell code (BEST) in cylindrical geometry with a perfectly conducting cylindrical boundary at radius  $r_w$ . Maxwell’s equations (21) and (22) are solved using fast Fourier transform techniques (FFT) in the longitudinal and azimuthal directions. The particle positions [Eqs. (24) and (25)] and weights [Eq. (26)] are advanced using a second-order predictor–corrector algorithm. The code is parallelized using Message Passing Interface (MPI) with domain decomposition in the direction of beam propagation. The NetCDF data format is used for large-scale diagnostic and visualization. Typical runs consist of  $10^6$  simulation particles and are performed on the IBM SP/RS 6000 at NERSC.

**IV. SIMULATION RESULTS**

Here we present the simulation results for an axially continuous, anisotropic beam in a constant focusing field. For simplicity we perform the simulations in the beam frame. It is assumed that the equilibrium distribution function is bi-Maxwellian and given by Eq. (1), where  $\hat{n}_b$  is the on-axis ( $r=0$ ) beam density, and  $T_{\perp b}$  and  $T_{\parallel b}$  are the transverse and longitudinal temperatures of the beam particles. The equilibrium self-field potentials  $(\phi^0, A_z^0)$  are determined

numerically from Maxwell’s equations.<sup>14–16</sup> It is also assumed that the beam is located inside a grounded, cylindrical, perfectly conducting wall at radius  $r_w=3r_b$ , where  $r_b=[\langle r^2 \rangle]^{1/2}$  is the rms beam radius. Random initial perturbations are introduced to the particle weights, and the beam is propagated from  $t=0$  to  $t=800\omega_f^{-1}$ .

The simulations are performed using the nonlinear  $\delta f$  simulation method described in Sec. III for a wide range of normalized beam intensities ranging from  $s_b=0.1$  to  $s_b=0.95$ , and detailed stability properties have been determined for the range of intensity parameters satisfying  $s_b \geq 0.5$  assuming axisymmetric perturbations with  $\partial/\partial\theta=0$ . Shown in Fig. 6 is the time history of the density perturbation  $\delta n_b = \int d^3p \delta f_b$  for normalized beam intensity  $s_b=0.7$ . The initial temperature ratio is taken to be  $T_{\parallel b}/T_{\perp b}=0.04$ . After the initial exponential growth phase, the instability saturates at a moderately large level with  $|\delta n_b^{\text{max}}/\hat{n}_b| \approx 0.05$ .

Figures 7 and 8 show plots of the real and imaginary parts of the complex oscillation frequency  $\omega$  vs normalized axial wave number  $k_z r_w$ . The instability has a finite bandwidth with maximum growth rate  $\text{Im } \omega/\omega_f \approx 0.02$  at  $k_z r_w = 7.5$ . For long wavelengths with  $k_z^2 r_w^2 \ll 1$ , the dispersion relation is linear with  $\text{Re } \omega$  proportional to  $k_z r_w$ . For short wavelengths with  $k_z^2 r_w^2 \gg 1$ , the transverse beam size is unimportant and  $\text{Re } \omega \approx 1.03\omega_f$ . The dependence of the maximum growth rate  $(\text{Im } \omega)_{\text{max}}/\omega_f$  on beam intensity  $s_b$  is shown in Fig. 9. The maximum growth rate  $(\text{Im } \omega)_{\text{max}}/\omega_f \approx 0.038$  oc-

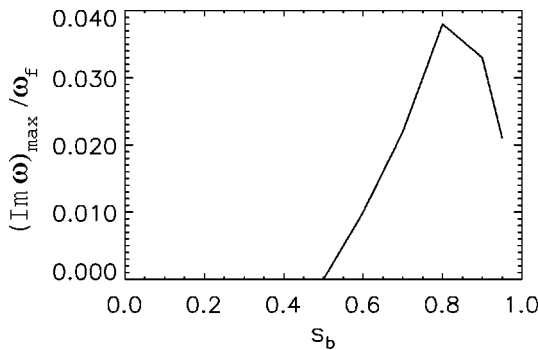


FIG. 9. Plot of  $(\text{Im } \omega)_{\text{max}}/\omega_f$  vs normalized beam intensity  $s_b$  for  $r_w=3r_b$ , and initial  $T_{\parallel b}/T_{\perp b}=0.04$ .

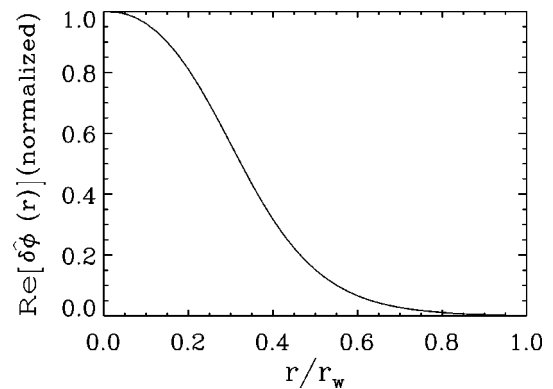


FIG. 11. Radial mode structure of the unstable eigenfunction for  $k_z r_w=7.5$ ,  $s_b=0.7$ , and  $r_w=3r_b$ , and initial  $T_{\parallel b}/T_{\perp b}=0.04$ .

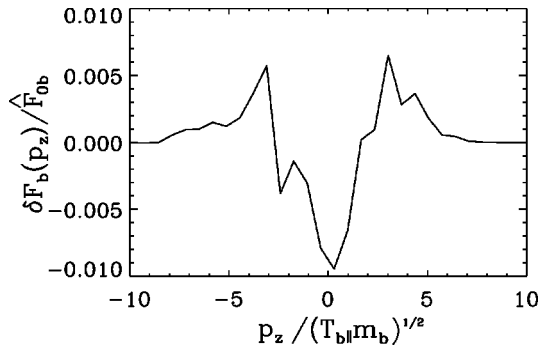


FIG. 12. Perturbed axial momentum distribution  $\delta F_b(p_z)/\hat{F}_{0b}$  at time  $t = 800\omega_f^{-1}$ , for normalized beam intensity  $s_b = 0.7$  and  $r_w = 3r_b$ , and initial  $T_{||b}/T_{\perp b} = 0.04$ .

curs for  $s_b \approx 0.8$ , with no instability in the region  $s_b \leq 0.5$ .

Figure 10 shows a plot of the real oscillation frequency  $\text{Re } \omega/\omega_f$  vs normalized beam intensity  $s_b$  for the unstable mode. The radial structure of the unstable mode is shown in Fig. 11 for  $k_z r_w = 7.5$ . Only the real part of the eigenfunction is shown, since  $\text{Im } \delta\phi \approx \text{const} \cdot \text{Re } \delta\phi$  for the weakly unstable mode. The simulation results presented in Figs. 6–11 are in good qualitative agreement with the theoretical model presented in Sec. II in terms of the mode structure and real oscillation frequencies (see Figs. 1–5). The difference in the absolute value of the growth rate  $(\text{Im } \omega)_{\text{max}}/\omega_f$  in Fig. 2 and Fig. 9, and the existence of the instability cutoff for large values of the normalized wavenumber in Fig. 8, are attributed to the Landau damping associated with the nonzero value of longitudinal temperature  $T_{||b}$  in the simulations.

The net change in the longitudinal momentum distribution  $\delta F_b(p_z)/\hat{F}_{0b}$  at  $\omega_f t = 800$  in the simulation is shown in Fig. 12. Here,  $\delta F_b(p_z) = \int d^2 p_{\perp} d^3 x \delta f_b$  and  $\hat{F}_{0b} = \hat{n}_b / (2\pi m_b T_{||b})^{1/2}$ . The formation of tails in the axial momentum distribution in Fig. 12 and the consequent saturation of the instability are attributed to quasilinear stabilization due to resonant wave–particle interactions in the tails of the distribution function.

Simulations have also been carried out for different values of temperature anisotropy  $T_{||b}/T_{\perp b}$ . Plotted in Fig. 13 is the ratio  $(T_{||b}^{\text{th}})^{1/2} k_z / m_b^{1/2} \omega_f$  vs normalized beam intensity  $s_b$ ,

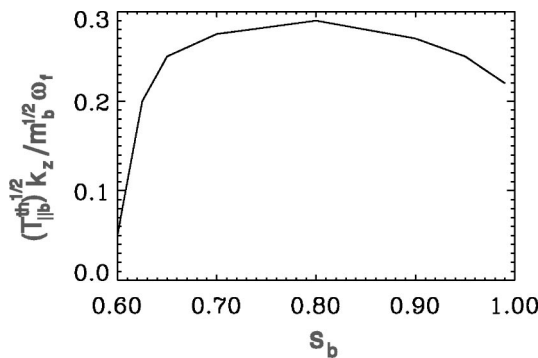


FIG. 13. Ratio  $(T_{||b}^{\text{th}})^{1/2} k_z / m_b^{1/2} \omega_f$  plotted vs normalized beam intensity  $s_b$  for  $r_w = 3r_b$ .

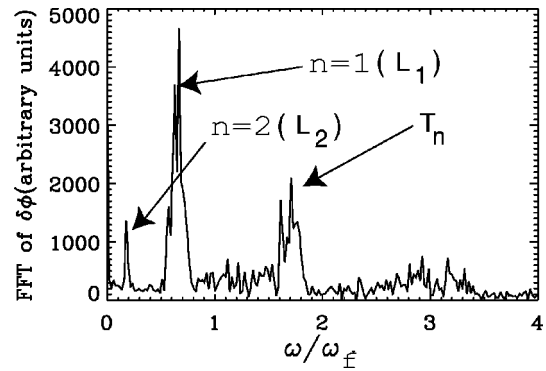


FIG. 14. Frequency spectrum of stable oscillations for  $k_z r_w = 3$ ,  $s_b = 0.8$ , and  $r_w = 3r_b$ .

where  $T_{||b}^{\text{th}}$  is the threshold value of longitudinal beam temperature for the onset of instability and  $k_z$  is the axial wave number.

The saturation mechanism due to resonant wave–particle interactions suggests that the instability is absent if the Landau damping rate due to nonzero thermal spread in the axial direction is greater than the instability growth rate for  $T_{||b} = 0$ . This implies that  $(T_{||b}^{\text{th}})^{1/2} k_z / m_b^{1/2} \omega_f \approx \gamma(T_{||b} = 0) / \omega_f$ , where  $\gamma(T_{||b} = 0)$  is the instability growth rate for  $T_{||b} = 0$ . In the present simulations, the instability is found to be absent if the ratio of initial axial and transverse temperatures is greater than the threshold value  $(T_{||b}/T_{\perp b})^{\text{th}} = 0.07$ .

Finally, we present simulation results for parameters in the stable regime for  $s_b = 0.8$  and  $k_z r_w = 3$ . The temperature ratio is taken to be  $T_{||b}/T_{\perp b} = 0.0025$ . Figure 14 shows the frequency spectrum, and Fig. 15 shows the real part of the eigenfunctions for the lowest frequency longitudinal modes. The frequency spectrum in Fig. 14 agrees reasonably well with the theoretical results in Fig. 4. Note from Fig. 14 that the spread in depressed betatron frequency  $\omega_{\beta\perp}(H_{\perp})$  results in a finite bandwidth to the frequency curves.

## V. CONCLUSIONS

To summarize, in Sec. II we generalized the classical Harris-type instability to the case of an intense charged particle beam with anisotropic temperature ( $T_{||b}/T_{\perp b} < 1$ ) including the important effects of finite transverse geometry

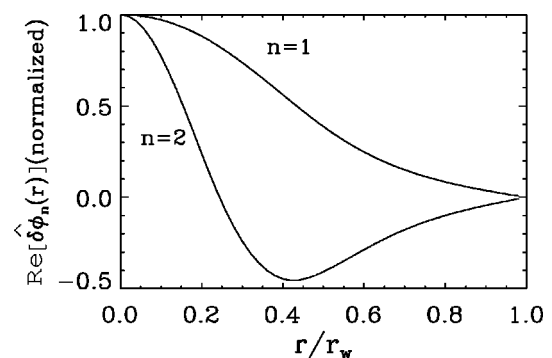


FIG. 15. Radial mode structure of the stable eigenfunction for  $k_z r_w = 3$ ,  $s_b = 0.8$ , and  $r_w = 3r_b$ .



and beam space-charge. Using the simplified assumption of negligible spread in depressed betatron frequency, we derived a simple dispersion equation for the lowest-order eigenmodes for the case of extreme temperature anisotropy ( $T_{\parallel b}/T_{\perp b} \rightarrow 0$ ). For sufficiently large values of  $k_z^2 r_b^2 \gg 1$ , where  $r_b$  is the rms beam radius, the analysis of the dispersion equation leads to a strong anisotropy-driven instability provided the normalized beam intensity  $s_b = \hat{\omega}_{pb}^2 / 2\omega_f^2$  is sufficiently large. In Sec. IV, the BEST code,<sup>14</sup> which implements the nonlinear  $\delta f$  scheme described in Sec. III, was used to investigate the detailed stability properties of intense charged particle beams with large temperature anisotropy ( $T_{\parallel b}/T_{\perp b} \ll 1$ ) assuming axisymmetric perturbations with  $\partial/\partial\theta = 0$ . The simulation results clearly show that moderately intense beams with  $s_b \gtrsim 0.5$  are linearly unstable to short wavelength perturbations with  $k_z^2 r_b^2 \gtrsim 1$ , provided the ratio of longitudinal and transverse temperatures is smaller than some threshold value. The mode structure, growth rate and conditions for the onset of the instability are qualitatively similar to what is predicted by the simple theoretical model presented in Sec. II. The main saturation mechanism for the instability is the resonant wave-particle interactions that occur during the formation of tails in the axial momentum distribution. In the nonlinear saturation stage, the total distribution function is still far from equipartitioned, and free energy is available to drive an instability of the hydrodynamic-type.<sup>21,22</sup>

## ACKNOWLEDGMENTS

It is a pleasure to acknowledge the benefit of useful discussions with Igor Kaganovich, Steve Lund, and Wei-li Lee.

This research was supported by the Department of Energy.

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